

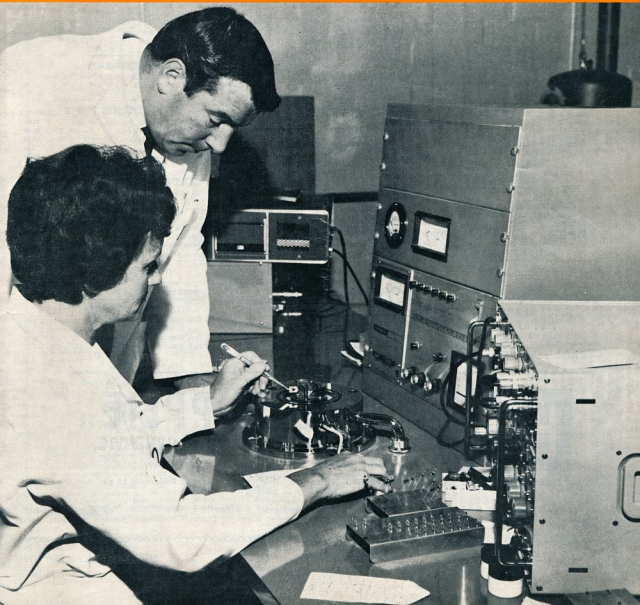
amateur radio

Vol. 38, No. 11

NOVEMBER, 1970

Registered at G.P.O., Melbourne, for
transmission by post as a periodical

Price 30 Cents



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Pocket Type, 1,000/OPV. AC Volts: 0-10, 50, 250, 1,000V. (1K/OPV). AC Volts: 0-10, 50, 250, 500, 1,000V. (1K/OPV). DC Current: 0-100 mA. Resistance: 0-150K ohms (2K centre). Two colour scale, Range Selector switch. Size: 3 1/2 x 2 1/4 x 1 inch.

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8A7	15 ohms	" "	\$7.20	"	40c
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amateur radio

JOURNAL OF THE WIRELESS INSTITUTE OF AUSTRALIA. FOUNDED 1910



NOVEMBER, 1970
Vol. 38, No. 11

Publishers:
VICTORIAN DIVISION W.I.A.
Reg. Office: 478 Victoria Parade, East Melbourne, Vic., 3002.

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Advertising Representatives:
TECHNICAL NEWS PUBLICATIONS
21 Smith St., Fitzroy, Vic., 3065. Tel. 41-4982.
P.O. Box 108, Fitzroy, Vic., 3065.

Advertisement material should be sent direct to the printers by the first of each month.

Hamads should be addressed to the Editor.

Printers:
"RICHMOND CHRONICLE," Phone 42-2419.
Shakespeare Street, Richmond, Vic., 3121.

★

All matters pertaining to "A.R." other than advertising and subscriptions, should be addressed to:

THE EDITOR,
"AMATEUR RADIO,"
P.O. BOX 36,
EAST MELBOURNE, VIC., 3002.

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Members of the W.I.A. should refer all enquiries regarding delivery of "A.R." direct to their Divisional Secretary and not to "A.R." direct. Two months' notice is required before a change of mailing address can be effected. Readers should note that any change in the address of their transmitting station must, by P.M.G. regulation, be notified to the P.M.G. in the State of residence; in addition, "A.R." should also be notified. A convenient form is provided in the "Call Book".

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COVER STORY

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The second price reduction is **YAESU MUSEN FL-2000B AMPLIFIER**, with imported American CETRON 572-B valves, now only \$350.

Also: **HY-GAIN TH6DXX** with balun, CDR Ham-M rotator plus 50 yards 8-cond. cable, one package \$400.

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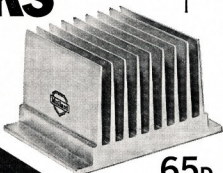
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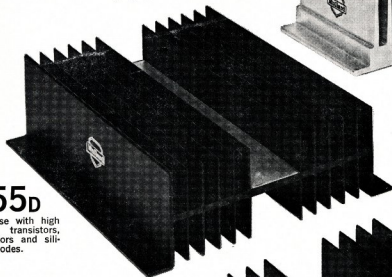
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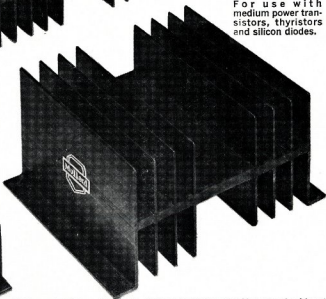


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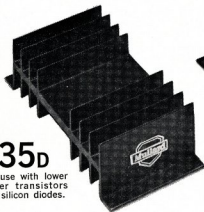
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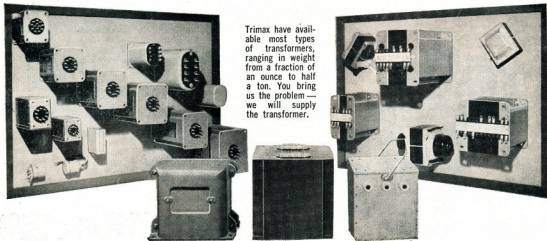
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LM 51



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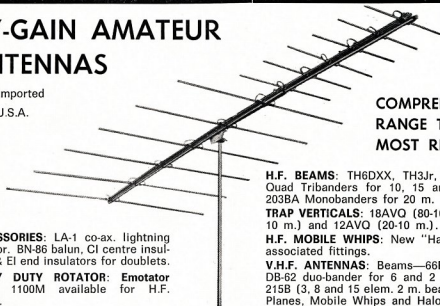
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COMMENT:
FEDERAL

"ONE IN A
MILLION"

If you are hungry, and cannot find work, or if you can and you will earn barely enough to feed yourself, and if you have never been to school—why should any hobby, let alone Amateur Radio interest you?

If you live in India and you are a Radio Amateur, you are literally "one in a million"—for in a population of 500 million people there are only some 450 licensed Amateurs.

Some of those 450 licensed Amateurs are by any standard well off. Most are not. Most are not active. They cannot compete with their equipment built with the components available to them, or with the s.s.b. stations of the rest of the world. Who works any a.m. stations on 20 metres these days? Of course components are not the only problem; I was repeatedly told while in India that hobbies are not in the blood of Indians—a hobby is an expression of a restless, seeking, Western society.

I.A.R.U. and we in our Regional organisation seek the development of Amateur Radio in countries like India. We seek to achieve this partly because we believe in what we do and we wish to share it, also partly because we believe that by contributing in some small way to the development of technology in countries like India we are doing something useful in the world around us, and partly for our own protection. It is the last point only that needs explanation.

India, to use it in the present context as an example, has, like us, one vote at International Telecommunications Union Conferences. Why should it vote to support Amateur Radio unless Amateur Radio is contributing something to its national life? The v.h.f. spectrum is a good illustration of the present development of our hobby in that country. In New Delhi I met an Amateur who is able to transmit and receive on 2 metres. There used to be two Americans and an Australian in New Delhi and together they formed a net on Sunday mornings. Now the two Americans and the Australian have left and the local Amateur awaits the appearance of someone else to talk to on 2 metres. Any frequency higher than 148 MHz. may as well not exist—in India you just cannot get the components to even try to make the equipment.

One in a million—that is the problem in India, and the problems of Amateur Radio in India are the problems of India. The two are inexorably intertwined. Is it even realistic to talk of National Amateur Radio Societies and

their international organisations rendering meaningful assistance? I do not believe that the solution lies in giving, for example, complete s.s.b. (and expensive) transceivers. This sort of charity obviously demonstrates that Amateur Radio is in fact a rich man's hobby. It teaches nothing and achieves little. The long term solution must be through the education system—such as it is. In India, education is not compulsory. This involves persuading those responsible for education that Amateur Radio as part of say, Science in clubs and schools, is a valuable tool for developing the technology of India.

Some individual Amateurs have had and have used their presence in India to assist Amateur Radio. One example is an Australian, Howard Ryder, VK-3ZJY. During his stay in India as a technical specialist working with the Colombo Plan, he taught other Amateurs how to build their equipment from locally-available products. He was the Australian who started the 2 metre net I have referred to. I do not know whether he will ever realise the affection that those who he assisted have for him. Repeatedly I was asked to ask him to return, and to tell him that they need him.

Amateur Radio needs more people like Howard Ryder in places like India—people who are prepared to work amongst Indians and to know the back streets of Chandnichowk, people who do not spend all their time in foreign lands at the bar of an intercontinental hotel.

There is room also for tangible assistance in the form of those components which are unavailable to India and which are essential to the production of equipment, such as s.s.b. transmitters.

A small boy who has never been to school and will never go to school, and who begs with head bowed while a taxi waits at a traffic light, will never be a Radio Amateur. But there are others who do attend school, who one day given the right training may become Radio Amateurs. It is these people that we must seek to influence. At the same time we lend encouragement to those who already are Amateurs to make sure that they persist with their hobby despite the difficulties that face them. Let us at the same time start at the top with those people who are capable of being Amateurs, and encourage them to become Amateurs and to encourage others to do likewise. Perhaps in our lifetime we may see in India "one in a quarter of a million".

—Michael J. Owen, VK3KI,
Federal President.

MODERN MODULATION SYSTEMS

R. F. DANNECKER,* VK4ZFD

The purpose of this article is to acquaint Amateurs with modulation systems using other than sine waves and continuous signals. Pulse amplitude modulation (p.a.m.), pulse width modulation (p.w.m.), pulse position modulation (p.p.m.) and pulse code modulation (p.c.m.) are discussed, and reasons for their importance outlined

In classical modulation systems, e.g. those represented by a.m., s.s.b., f.m., a continuous message signal is transformed into a modulated transmitted signal which is also continuous (see Fig. 1). Modern modulation systems could be called discrete communication systems. In a discrete system the continuous message signal is transformed into a discontinuous modulated signal. The discontinuities can be of two forms, either discontinuities in amplitude or discontinuities in time.

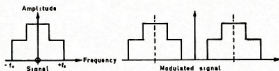


FIG. 1. CLASSICAL MODULATION (D.S.B.)

(Note that both signals are continuous.)

The foundations for such systems were laid by C. E. Shannon working in the Bell Telephone Laboratories (about 1949). Shannon showed that if a normal (bandwidth limited to $\pm f_0$) signal is sampled at (or above) a certain rate, and the sampled values transmitted; the original signal can be reconstructed exactly from the sampled signal. The importance of this result is the word **exactly**. It can be shown that the sampling must take place at a frequency equal to or greater than twice the maximum frequency in the signal (f_0) for this to be true.

Sampling can be achieved by opening a gate (see Fig. 2) at the required rate by a waveform consisting of a series of "spikes". Fig. 3 shows the process. Thus we obtain the simplest form of discrete communication system, namely pulse amplitude modulation (p.a.m.).

In fact the frequency spectrum of the sampled signal is a repeated version of the original signal, the amount of separation between the repeated versions depending on the sampling rate. If the sampling rate is at $2f_0$ this is known as the Nyquist ("high-kwist") rate. The period between successive spikes is one nyquist interval. The effect of sampling rate on the spectrum of the sampled signal is shown in Fig. 4. In 4(b) sampling greater than the nyquist rate the repeated spectra are well separated. In 4(c) sampling at the nyquist rate the repeated spectra just touch. In 4(d) sampling at less than the nyquist rate, the repeated spectra overlap.

As stated previously, the original signal can be recovered. This is done by passing the sampled signal through a low pass filter which cuts off at frequency f_0 (see Fig. 5). If the sampling were at or greater than the nyquist rate, the original signal has been recovered exactly. If the sampling were at less than the nyquist rate, the distortion introduced by overlapping of the spectra cannot be removed.

This may seem of academic interest only since p.a.m. would appear to offer

no obvious advantage over classical modulation. In practice, because of the ease with which this form of modulation may be obtained, it is often the first step in a discrete modulation system. Other forms of modulation are obtained by electronic processing of the p.a.m. wave. One such form is shown in Fig. 6(b). In this form, the pulses are of constant height, but their widths are proportional to the signal ampli-

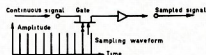


FIG. 2. SAMPLING SYSTEM.



FIG. 3. SAMPLING OF CONTINUOUS SIGNAL.

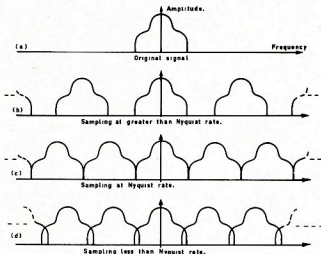


FIG. 4. EFFECT OF SAMPLING ON SPECTRUM.

* 52 Pohlman Street, Southport, Qld., 4215.

tudes at the sampling times. This form may be obtained from pulse amplitude modulation by passing through an amplitude to time converter. This second form of discontinuous modulated signal is known as pulse width modulation (p.w.m.).

If a p.w.m. wave were differentiated, the form shown in Fig. 6(c) would be obtained. The positive going pulse at the leading edge of each pulse contains no information and so could be removed, leaving the negative going pulses shown inverted in Fig. 6(d). In this form of modulation it is the position of the pulse which ultimately reflects the amplitude of the originating signal. This form is called pulse position modulation (p.p.m.).

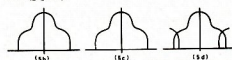


FIG. 5. EFFECT OF LOW PASS FILTERING ON FIG. 4

A fifth form of discrete modulation which requires more consideration than the previous types is obtained if we take each pulse height in a p.a.m. wave and convert this amplitude into a binary number representing the height.

[The binary numbering system involves powers of 2 while the common system involves powers of 10, e.g. one hundred and sixty-five in the decimal system would be represented as:

$$\begin{aligned} &1 \times 10^2 + 6 \times 10^1 + 5 \times 10^0 \\ &= 1 \times 100 + 6 \times 10 + 5 \times 1 \\ &= 100 + 60 + 5 \\ &= 165 \end{aligned}$$

in the binary system this would be represented as:

$$\begin{aligned} &1 \times 2^7 + 0 \times 2^6 + 1 \times 2^5 + 0 \times 2^4 + 0 \times 2^3 + 1 \times 2^2 + 0 \times 2^1 + 1 \times 2^0 \\ &= 1 \times 128 + 0 \times 64 + 1 \times 32 + 0 \times 16 + 0 \times 8 + 1 \times 4 + 0 \times 2 + 1 \times 1 \\ &[= 128 + 0 + 32 + 0 + 0 + 4 + 0 + 1] \\ &= 1 \quad 0 \quad 1 \quad 0 \quad 0 \quad 1 \quad 0 \quad 1 \end{aligned}$$

The advantage of the binary system from an electrical viewpoint is that a number can be represented as a sequence of ON or OFF states rather than by a sequence of 10 discrete levels as would be required for a decimal representation.]

Thus a pulse of height 13 volts might be represented by the number 01101 and a pulse of height 20 volts by the number 10100. A different form of modulation would then be obtained if instead of sending a single pulse in each nyquist interval, a sequence of say five pulses were to be sent during that time with each pulse being either a one or a zero, so as to form the binary number representing the original sampled height in that nyquist interval. In this form the sample heights have been encoded into binary numbers and the form is referred to as pulse code modulation (p.c.m.).

It is necessary to limit the number of pulses in the sequence due to practical considerations. If we allow five pulses in each nyquist interval to repre-

sent the amplitude of the pulse, then the maximum number of possible different levels which can be distinguished will be $2^5 (= 32)$. Suppose the maximum voltage in the signal is say 32 volts; suppose also the amplitude of the actual signal at successive sampling times is as shown. Then the binary number (given in decimal form) closest to each amplitude will also be as shown in Table 1.

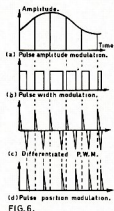


FIG. 6.

In fact the net effect of this finite number of quantisation levels is the same as if noise were added to the original signal. By analogy with this case, the error is referred to as the quantisation noise. Quantisation noise is an additive noise, similar to naturally occurring noise due to atmospheric, etc., in standard communications systems. However, just as the addition of

natural noise prevents the exact recovery of a signal, so the addition of quantisation noise also prevents an exact representation of the original message being obtained. Quite obviously the quantisation noise can be reduced by increasing the number of pulses in each sequence. This means that an improved signal will then occupy more bandwidth than previously.

Nyquist Interval	t0	t1	t2	t3	t4	t5	t6	t7
Actual Amplitude	20.0	19.1	16.5	12.8	3.2	7.7	14.9	6.4
Sample Amplitude	20	19	17	13	3	8	15	6
Error	0	-0.1	+0.5	+0.2	-0.2	+0.3	+0.1	-0.4

Table 1.

It can be shown that the capacity of a communications system is given by:

$$C = W \log_2 (1 + \text{SNR})$$

where C = capacity of system

W = bandwidth

$$\text{SNR} = \frac{\text{signal-to-noise ratio}}{\text{noise power}}$$

It is clearly seen that given the value of signal-to-noise ratio and bandwidth W, the capacity C of the system is determined. Should this capacity not be sufficient for some particular purpose (e.g. high speed data), then either the SNR must be increased by increasing the signal power which is transmitted, which may not be possible, or W must be increased. Increase of bandwidth W is sometimes the only means of increasing system capacity (e.g. spacecraft). There are a variety of ways used to increase W. (In classical modulation f.m. occupies more bandwidth than a.m.) In particular, conversion of the signal into any of the pulse modulated forms which we have considered will result in an increase, so that for a given noise level, the fidelity (readability) of systems employing this method is inherently better than would be obtained if the original signal were say amplitude modulated. This is one reason for the increasing modern use of these methods.

In practice the encoding of p.c.m. can be modified in a number of ways.

To properly decode a p.c.m. sequence (word), the receiver must know the position of the start of each word, or it may decode bits from two adjacent words. To overcome this, a few bits are added at the start of each word, which have a fixed waveform and can be easily recognised. These bits comprise the "synchronisation code," and provide word synchronisation. The total number of bits per nyquist interval must then be greater than the number required to give the amplitude of the signal at that time. The complete sequence, synch bits plus information bits, is called a "frame." (See Fig. 7.)



FIG. 7. PULSE CODE MODULATED SIGNAL.

In cases where additive natural noise is present, errors in the received signal will occur, i.e. a 1 may be detected as an 0 or vice versa. This effect can be reduced if to the information and synch bits are added what are known as par-

ity check bits. These check bits are calculated on the information bits, e.g. parity check bits are set at 0 if the checked information bits contain an even number of ones and are set to 1 if the information bits have an odd number of ones. If information bits are then altered during transmission, the even-odd correspondence with parity check digits will be altered. This should be detectable by comparing parity checks with information bits, and the bits in error can be corrected. A code containing parity check bits in this way is an "error correcting code".

A further advantage arises in the use of a binary coding system in that the receiver has only to decide if an incoming signal is a 1 or a 0 rather than some particular level out of a large number of possible levels. The detector can be a simple level detector to give zero output if the incoming signal is below a certain level corresponding to a 0 and

to give an output if the incoming signal is above this level corresponding to a 1. Obviously such a system can be made very accurate even for low SNR and the process can be improved further by the use of optimum or Wiener filtering in the system.

In conclusion it should be pointed out that a practical p.c.m. system is quite complex and, at least for the present, is beyond the financial reach of most Amateurs. Much research is being carried out into p.c.m. and in the future its use will become increasingly widespread.

I should like to acknowledge the valuable assistance given in the preparation of this article by Dr. L. V. Skatberol of the Department of Electrical Engineering, University of Queensland.

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PROVISIONAL SUNSPOT NUMBERS

JULY 1970

Dependent on observations at Zurich Observatory and its stations in Locarno and Arosa.

Day	R	Day	R
1	137	16	61
2	153	17	59
3	155	18	56
4	159	19	92
5	165	20	92
6	161	21	130
7	125	22	122
8	115	23	106
9	104	24	116
10	90	25	122
11	81	26	136
12	74	27	153
13	79	28	146
14	68	29	153
15	61	30	122
		31	108

Mean equals 112.5

Smoothed Mean for January 1970: 106.2

Predictions of the Smoothed Monthly Sunspot Numbers

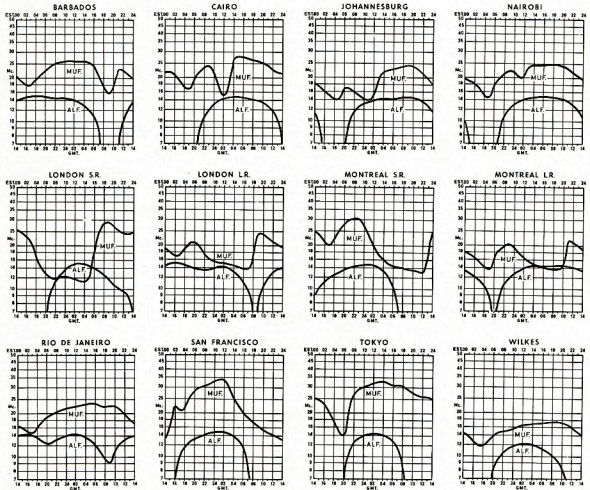
August	85	November	88
September	83	December	87
October	91	January	85

—Swiss Federal Observatory, Zurich.

AMATEUR FREQUENCIES:
USE THEM OR LOSE THEM!

PREDICTION CHARTS FOR NOVEMBER 1970

(Prediction Charts by courtesy of Ionospheric Prediction Service)



Doing Your Own Transistor Tests

LARRY ALLEN

To hear some guys tell it, a transistor is the easiest thing in the world to test. But others don't agree. A transistor to them is still a mystery.

Well, the truth is, most transistors can be tested without complicated equipment, gimmicks, calculations, or formulae. To keep it simple, there are just two basic things you need to find out about a transistor: (1) Does it work at all? (2) How well?

TRANSISTOR PARAMETERS

That word "parameters" scares off a lot of Hams. It conjures up complicated graphs with bent lines and long formulae with Greek symbols and big and little letters. All the word actually refers to is **conditions of operation**.

One transistor manual lists 103 possible parameters. They're great for a transistor designer. But a lot fewer is plenty for testing on the repair bench. In fact, I won't even use the term "parameters". Instead, I'll just tell you about the voltages, currents and resistances that tell you how a transistor is doing.

I'll start with the diagram of a simple transistor stage in Fig. 1. This is a grounded-emitter amplifier—probably the most common transistor stage in use today.

The transistor is NPN. Bias is forward when the base is slightly positive with respect to emitter. The collector is "far" positive with respect to emitter.

A PNP transistor takes negative voltage on the base to forward bias the emitter-base junction. That's not necessarily a negative voltage to ground, but to emitter. The collector of a PNP operates "far" negative from the emitter.

WHICH WAY IS UP?

Some Hams I've talked to about transistors seem confused by operating voltages. One key to understanding is knowing how to describe the voltages.

For example, in Fig. 1 if the base voltage changes to 0.1 volt, it has obviously become less positive. That means less positive with respect to wherever you're measuring from, and for most measurements that is ground.

Look at the same voltage with respect to the emitter. As it's labelled on the diagram, the base is normally more

positive than the emitter by about 0.3 volt. (The emitter is 0.15 volt, and the base is 0.45 volt; between the two is 0.3 volt, the base more positive than the emitter.)

Know what that means? "More negative" is exactly the same thing as "less positive". And "more positive" means the same as "less negative".

If the base voltage in Fig. 1 drops to 0.1 volt, the voltage relationship between base and emitter changes. The difference is then 0.05 volt (0.15 minus 0.1 equals 0.05), but the base has become **less positive** than the emitter. That's the same as saying it is **more negative** than the emitter. The emitter-to-base bias has become 0.05 volt negative. (Call it emitter-base bias, not base-emitter bias. You want the emitter as the point of reference, so name it first.) An NPN transistor with the base negative is reverse-biased. Collector current can't flow.

This should make clear that, even though you measure voltages with your voltmeter common lead connected to ground, the important thing is the voltage between elements of the transistor. In most transistor stages, your chief interest is the voltage between emitter and base; of secondary interest is the voltage between emitter and collector.

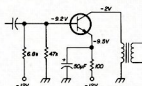


Fig. 2.—Changing polarity of power supply doesn't alter circuit arrangement or operation.

Suppose someone tells you the base voltage on one of these transistors has "gone up". What does that really mean? Usually he means the voltage is higher in the polarity shown on the schematic.

Consider the base voltage in Fig. 2. It appears "lower" than the emitter voltage. Its value is less. Measured to ground, the base voltage is less negative than the emitter voltage. The important thing is this: being less negative, the base is **more positive** than the emitter. That provides forward bias for any NPN transistor.

If the base voltage goes up—that is, if it goes further negative with respect to ground, as the voltmeter measures—the bias actually decreases. Say the meter measures —9.4 volts. The base has become **more negative** than it was. Looking from the standpoint of emitter-base bias, it tells you more if you say bias has become **less positive**. Forward bias is therefore reduced. Your voltmeter thus shows base voltage higher than before, but bias is less.

These are important relationships in transistor repair work. The simplest way to combat this seeming ambiguity is to quit using such vague notions as "up" and "down" for voltage measurements. Form the habit of thinking more negative or less negative, more positive or less positive.

TESTS THAT REVEAL

At the repair bench you are usually concerned with a transistor in some piece of equipment. Tests you can make without unsoldering the transistor are the handiest.

There are three ways to evaluate a transistor in that circumstance. Two additional tests can be made if you unsoldered one or two transistor connections.

Finally, two quick test procedures evaluate a transistor outside the circuit. They are especially handy if you have a batch of unidentified transistors you want to check out. Even these tests can tell you more about transistor quality than you might expect.

VOLTAGE MEASUREMENTS

Once you examine d.c. flow in transistor stages, you can figure out a lot from the voltages. If a voltage is wrong, deduction can tell you whether it's the transistor or something external.

Pretend the stage in Fig. 3 is giving you trouble. Your voltmeter tells you the base actually has —5 volts on it instead of the low —0.45 volt that's normal. Think out the possible causes.

Could be one of the base resistors is bad. But collector-base leakage in the transistor is far more likely. You can verify by disconnecting the base lead of the transistor. If voltage on the open base lead is still highly negative, the transistor junction is leaky.

Or, in the same stage, suppose the emitter measures —0.9 volt. For some reason, more current than normal is flowing in the 52-ohm resistor the emitter voltage is measured across. The transistor is probably drawing too much current.

But is that due to overbias or a transistor defect? If base voltage has remained about the same, the trouble is likely in the transistor. You see, —0.9 volt at the emitter, with only —0.45 volt at the base, constitutes reverse emitter-base bias for this PNP trans-

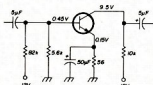


Fig. 1.—Common-base transistor amplifier is popular in Amateur equipment.

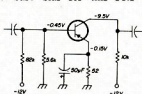


Fig. 3.—PNP transistor in this basic amplifier works the same as Fig. 1; only change involves voltage polarities on the various elements.

* Reprinted from "Ham Radio," July 1970.

sistor. That would reduce current through the transistor, not increase it—unless the transistor happens to be defective.

There are plenty of other examples of this kind of reasoning. Just remember which polarity of transistor you're dealing with and the likely effects of voltage changes. And don't forget to interpret voltage measurements in terms of their relation to each other and to the transistor itself.

The other two in-stage test ideas utilise a transistor's bias characteristic. For most transistors, zero and reverse bias cause zero collector current. A healthy forward bias assures significant collector current. These precepts of course apply only if the transistor is not defective.

The first test is for stages in which the transistor operates with forward bias. You can determine that from the schematic. Remember, forward bias is base-positive for an NPN transistor and base-negative for a PNP.

Connect your voltmeter at one of the points shown in Fig. 4. Several possible connections are illustrated. If you need it, you can insert the 100-ohm resistor;

For instance, the NPN transistor in Fig. 4A has forward bias only when the base is more positive than the emitter. How do you make it more positive? One way is to reduce the value of the supply resistor, since it goes to a positive voltage source. Just bridge it with a low-enough resistance to make the base more positive than the emitter. If the transistor is working normally, the voltmeter shows more collector current.

In Fig. 4B the basic supply scheme is different. But the transistor is still NPN. Forward bias requires base to be more positive than emitter, same as always. But how can you make it that way? Just remember that more positive is the same as less negative. Bridge a lower resistance from base to ground, low enough to reduce the base voltage to a value less than at the emitter. Collector current goes up. If not, the transistor isn't responding as it should.

The transistor in Fig. 4C is PNP. Forward bias demands a base more negative (less positive) than the emitter. It should by now be easy for you to figure how to make this base less positive. When you do, the voltmeter should register higher collector current.

there should be almost non-existent. Unwanted leakage lets current across the junction to the meter.

TESTING OUT-OF-CIRCUIT

If you have a transistor tester, fine. With a good one you can test transistors in or out of the stage faster than with the tests I've outlined here. But if you don't have one, you may often need these procedures.

Tests outside the stage are popular with Hams. The basic instrument is your ohmmeter. There are two main purposes. One is identification. The other is evaluation.

Hams often pick up transistor "bargains". You met a handful of odd-lot transistors, often unmarked or marked in some way that means nothing to you. You may not even know which wires go to emitter, base, or collector. Here's how to settle these doubts.

An ohmmeter with 1.5 volts or less between the test leads is safest (measure with some other voltmeter). More voltage might pop a transistor junction. Also, notice which test lead has the positive voltage and which the negative; you'll need to know for these tests. Nowadays, it seems most ohmmeter batteries are connected with positive voltage on the common or black test lead.

Pick any two transistor wires. Clip the ohmmeter to them in first one direction and then the other. If you get no reading, try another pair, again measuring in both directions.

When you get a low ohms reading (150 or less), one of the ohmmeter leads is clipped to the base wire. The way most transistors are arranged, it is the wire in the middle.

But you can make sure. Leave one ohmmeter lead clipped to the wire you think goes to the base. Move the other lead to the remaining transistor wire. If the ohmmeter reading is again low, the lead you didn't move is definitely clipped to the base. If not, the one you moved was.

You can now identify the transistor type. When you get low readings to both other elements with the positive ohmmeter lead connected to the base, you are testing an NPN transistor. A PNP transistor gives low readings when the negative ohmmeter lead is clipped to the base.

You've identified the base, but you don't know which of the other two wires goes to the collector. There were clues in years past, but you can't trust the dots, stripes, and tabs on today's myriad of transistors. And basing diagrams aren't standard enough to help much either.

Start with the ohmmeter connected to show low resistance between the base and either of the other elements. You know which wire is base, so unclip that lead and move it to the other unidentified wire. The meter should read infinity or open. If not, the transistor is defective.

Then click the range switch of your ohmmeter to higher scales until you see a slight downward meter deflection (something less than infinity). This usually happens on the Rx10K or Rx100K range. Next, reverse the two ohmmeter leads. The ohms reading will

(continued on page 16)

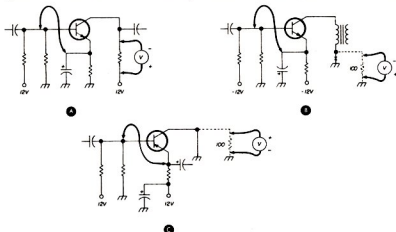


Fig. 4.—Voltmeter connections in several amplifier stages for making bias-change operation tests. Idea is to eliminate bias on stages that normally use forward bias and add it to those that don't, while watching the change in collector current. You can add a resistor if the collector circuit doesn't have one.

its value won't bother the circuit much. Indirectly you are measuring collector current.

Notice the voltmeter reading. Then clip a shorting jumper between base and emitter. The voltmeter reading should drop to almost nothing. If it doesn't, the base isn't controlling collector current.

The second test is for stages where zero or reverse bias is normal. (The transistor may conduct, but probably during only a small portion of each signal cycle, leaving an average or d.c. bias that is zero or reverse.) The voltmeter connections are the same as in Fig. 4.

This time, instead of eliminating bias by shorting base to emitter, you apply a definite forward bias to base. Figure out from the schematic what would constitute forward bias for the transistor. Then somehow alter the bias to make it temporarily forward. The meter reading should take a definite move upward, signifying more collector current.

DETECTING ABNORMAL LEAKAGE

Those tests let you know a transistor can control its collector current. That's the key factor. But there's another factor that can keep a transistor stage from performing up to par. You need a way to check leakage.

Basically, it's easy. Your voltmeter and soldering gun are the only equipment you need.

The leakage that can most upset stage operation is from collector to base. The collector junction of an operating transistor has a high reverse bias. If that junction lets "carriers" through in the wrong direction, transistor gain is poor.

To measure collector-base leakage, disconnect only the base lead of the transistor. Clip the voltmeter common lead to the emitter. Set the voltmeter as if you were measuring collector voltage. Touch the other test lead to the free end of the base lead. Voltage

An Outside Broadcast Amplifier

C. A. CULLINAN,* VK3AXU

LECTURE NO. 9

The original 3CS O.B. Amplifier No. 4 was manufactured in 1960 and after considerable work it could no longer meet the Australian Control Board's standards.

It was decided, therefore, that as part of our training programme that this amplifier would be dismantled and a new one built to take its place, the work to be done by our Cadet and to correspond with the appropriate part of the Marconi School course. The new amplifier would use as many components as possible from the old amplifier but would be different in mechanical construction and somewhat different in circuitry to avoid making a direct copy, as it was felt that little was to be gained in tuition in making a copy.

DESIGN AND NOTES

A single channel Outside Broadcast Amplifier to be built using valves and operated from the a.c. mains.

The amplifier must meet the Australian Broadcasting Control Board standards, and, where applicable, Australian Post Office specifications.

The only suitable output transformer, which was available, was an A. & R. type OT2629 for which a manufacturer's test certificate was held (22/4/69), in respect of A.P.O. Specifications 1053 and 1054.

Details of this transformer are:

Primary Impedance: 7,000 or 5,000 ohms, single ended.

Secondary Impedance: 500, 250 or 125 ohms.

Power Rating: 5 watts.

Frequency Response: 50 Hz. to 30 KHz. ± 2 dB.

Output Valve

The output transformer is suitable for use with any valve requiring a plate load of 5,000 or 7,000 ohms, and taking a plate current of 50 mA. Thus the choice falls mainly between types EL84/6BQ5, 6BM5, 6CW6 or 6V6GT. As a large number of EL84s are used in studio equipment, this type was chosen as the output valve, with 160 ohm cathode bias resistor. A simple resistor of this value was not available so some calculations were made to determine which of two 3 watt w.w. resistors on hand would give the necessary value when used in parallel. The two resistors selected were 250 ohms and 450 ohms, which in parallel become 160.7 ohms.

Other Valves

In order to meet the specified noise figures it is essential that the other valves must be of very low noise type and for this reason EF86 valves were selected. This type was first available in Australia somewhere in late 1954 to 1955. It is also known as 6BK8/7279, and was specifically designed for use in low level microphone or pick-up pre-amplifiers. It uses a 9-pin minia-

Continuing the series of lectures by C. A. Cullinan, VK3AXU, at Broadcast Station 3CS for students studying for a P.M.G. Radio Operator's Certificate.

ture base, has internal shields and a specially constructed heater-cathode system.

It is possible with proper design of equipment to reduce hum and noise voltages, referred to the control grid, to the order of 1.5 μ V. for hum and 2 μ V. for valve noise for an audio frequency bandwidth of 15 KHz.

In recent years an improved EF86 has made its appearance. For this valve, the previous mesh type anode (plate) has been replaced with a solid one. This gives additional shielding and reduces pick-up of external magnetic fields (hum) by as much as 6 dB.

It would appear that the EF86 is a later development of the valve type EF40.

For many years the designer has used EF86 valves as pentode audio frequency amplifiers with a plate load of 0.22 megohm, a screen resistor of 1 megohm, and a cathode resistor between 2,200 ohms and 3,000 ohms. With a cathode current not in excess of 1 mA. and cathode bias not less than 1.6 volts, excellent gain, low distortion and low noise have been achieved for a bandwidth of 15 KHz.

If they are available, the student is referred to the following publications for further details of the EF86/6BK8/7279 valve:

Radiotronics, Vol. 20, No. 6, June 1955.

Radiotronics, Vol. 22, No. 5, May 1957.

Mullard Circuits for Audio Amplifiers.

Philips Valve Data Handbook.

Calculations showed that with a microphone transformer having a turns ratio of 1:44.7 and a 6 dB. attenuator between the output transformer secondary and the amplifier output terminals, the specified gain of 80 dB. could be obtained by using two resistance coupled EF86 valves and an EL84 output valve, whilst applying considerable feedback over the last two stages.

Thus the amplifier portion of the design resolves itself into a three-stage amplifier, using EF86s in the first two stages with an EL84 in the output stage. Negative feedback to be used from the plate of the output valve to the cathode of the second valve.

Because the specifications state that the output of the amplifier is to be balanced and floating, it is not possible to use negative feedback from the secondary of the transformer. Also, the particular output transformer does not have a tertiary winding for feedback

purposes, therefore the feedback was taken from the plate (anode) of the output valve.

The input transformer is of the specially shielded type made for low level applications. The heavy shielding reduces hum pick-up as much as 40 dB below that picked up by a similar, but unshielded transformer.

The gain control is located, electrically, between the first and second stages.

POWER SUPPLY

The specifications stipulate that silicon diodes are to be used as rectifiers in the power supply.

S.T.C. EM410 silicon diodes were used as they were in our stock of spare parts. These diodes have the following characteristics as abstracted from an S.T.C. I.T.T. Application Note:

Peak inverse voltage (p.i.v.), 1,000 volts.

Average rectified current at 85°C., 0.5 amp.

Operating and storage temperature range, -55°C. to +135°C.

Voltage drop approx., 1.2 volts.

Consideration was given to the use of an Ironcore T5/102 power transformer which was available and was suitable. The following information was extracted from the maker's data sheet:

H.t. secondary voltage, 225-0-225, i.e. 225 volts each side of the centre tap.

H.t. secondary current, 50 mA.

Heaters, 6.3 volts at 2 amp.

An astatic shield is fitted between primary and secondaries to reduce capacitive coupling between these windings. In addition, it has an external eddy-current shield.

As the h.t. secondary has a centre tap, this means that a full wave rectifier circuit must be used.

Having selected the power transformer and the type of silicon diodes, it becomes necessary to determine how many diodes will be needed.

The term peak inverse voltage means the peak voltage that the rectifier can withstand in the reverse direction before it breaks down. This voltage includes both a.c. voltage and the d.c. output voltage.

Other terms used in place of peak inverse voltage are crest working reverse voltage (v.r.w.m.) and peak reverse voltage (p.r.v.). They all mean the same thing.

Now one of the characteristics of silicon diodes is that they are very liable to break down the moment the p.i.v. is exceeded. Some will be destroyed instantly, but others will recover if the excess is not too great.

Again from S.T.C.-I.T.T. Application Note, we take the information to enable us to determine the various voltages to be expected.

P.i.v. = 3.14 \times volts out.

V.r.m.s. = 1.11 \times volts out.

Volts out = volts r.m.s. \div 1.11.

* 6 Adrian Street, Colac, Vic., 3250.

Volts r.m.s. is the r.m.s. voltage from the h.t. centre tap to either high voltage end of the h.t. secondary winding.

Now let us do some calculations.

The a.c. r.m.s. voltage across one half of the h.t. secondary is 225 volts. Therefore the d.c. output voltage will be:

$$225 \div 1.11 = 202.7 \text{ volts}$$

and the p.i.v. will be:

$$202.7 \times 3.14.$$

However, this is for a choke input filter, but when a large condenser is connected across the output of the filter and the power supply is switched on, the output voltage will be much higher until the filter input condenser becomes fully charged and the valves have warmed up.

At the instant of "switch on" there is practically no load on the power supply so the output voltage of the rectifier system soars considerably.

In this amplifier the measured d.c. output from the rectifier at "switch on" was 340 volts.

For safety, it is necessary to take this new voltage as the d.c. output voltage (when the amplifier is warmed up this voltage will drop to 250v.).

Therefore the p.i.v. will be:

$$340 \times 3.14$$

$$= 1,067.6 \text{ volts.}$$

To allow for variations in a.c. mains voltages, also switching transients that may show up in the a.c. mains, it is desirable to add at least 25% to this value, i.e. $1,067.6 + 266.9 = 1,334.5$ volts.

The simplest way to accommodate this voltage is to put two diodes in series in each leg of the transformer. We selected EM410 diodes as they are rated at 1,000 p.i.v.

When a large condenser is used at the input of the power supply filter it is necessary to protect the diodes from burning out due to excess current through them as the rectifiers start to charge the condenser.

To avoid this problem, it is necessary to use a transformer having sufficient impedance to restrict this current flow or to put resistance in series with each h.t. leg of the transformer.

In this design, the 80 μ F. condenser is not excessively large and the impedance of the power transformer keeps the current within the limits of the diodes.

One problem of putting diodes in series is that sometimes they will not share the voltage between them, therefore a 1 megohm 1 watt resistor is wired across each diode.

PRACTICAL NOTES

The lead from the microphone transformer to the grid of the first EF86 was made as short as possible and shielded with braid fitted loosely to reduce the capacity between the lead and the braid.

A piece of $\frac{1}{4}$ " o.d. co-axial cable was used as the lead between the 0.022 μ F. coupling condenser and the top of the gain control, which was about 4" above the top of the chassis. The braid was earthed as close to the 0.022 μ F. con-

denser as practicable. The other end of the braid was connected to the "earthy" end of the gain control. The gain control was not earthed in any other manner.

The lead from the arm of the volume control to the grid of the second valve was also a piece of co-axial cable, with its braid earthed as close to the grid as possible. At its other end the braid was insulated so that it could not touch anything.

All these precautions were taken to reduce, as far as possible, frequency loss at the higher frequencies.

As part of tuition, the co-axial cable was replaced with tightly woven shielded wire. The frequency response at 10 KHz. immediately dropped to 5 dB. below that of 1 KHz.

Heater leads: The heater leads between the EF86s and the EL84 were twisted and shielded, also care was taken in the layout so that no heater lead passed near a grid pin in a valve socket.

Headphone Jack: This was insulated from the chassis to maintain a floating output as specified. Two 560 ohm resistors prevent a short circuit across the amplifier output should the headphones plug not be properly inserted.

Layout: An aluminium chassis was used to reduce hum transfer from the power transformer to the input transformer, as could happen with a steel chassis.

The power transformer was mounted in a rear corner of the chassis. The location of the output transformer was determined as follows:

After carefully insulating leads, a.c. power was fed to the power transformer to energise it.

Then a 7,000 ohm resistor was wired to the 7,000 primary of the output transformer and the 500 ohms secondary was connected to the A.W.A. Noise and Distortion Meter.

The 50 Hz. (hum) pick-up from the power transformer was measured with the N. & D. meter, after which the transformer was moved over the surface of the chassis to locate the position of minimum hum.

The location of the microphone input transformer was determined in a similar manner, using the high impedance input to the N. & D. meter connected to the transformer secondary, the primary being terminated with a 47 ohms 1 watt resistor.

Locating the transformers in this manner proved to be most successful as no hum can be detected in the completed amplifier.

The amplifier was fitted into a metal case, with carrying handles.

It is a matter of great satisfaction that the completed amplifier meets all the designed specifications and is a welcome addition to the station's O.B. equipment.

★

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ANTENNA FARMING

A. J. C. THOMPSON,* VK4AT

A 10 element long type Yagi on 7 MHz—a.m. at s.s.b. strength.

The reaction to the above circumstances have followed a fairly set pattern. Some were expected, some should have been expected, some were quite unexpected. From the reports received, the following are fairly representative:

- (1) The fact that it is a.m.
- (2) The unexpected strength.
- (3) The good quality of the transmission (where the gear was capable of judging it).
- (4) The way it bashed down the QRM.
- (5) Its good effect on QSB.
- (6) Its effect on the background noise level.

In addition to the above, the most interest was taken in:

- (1) The number of elements used on 7 MHz. (10 or 13).
- (2) The low height (20 feet poles).
- (3) The use of steel wire.
- (4) The valley QTH.
- (5) Why such a scheme was attempted.

I will try and get things straight right here. This article cuts no new ground scientifically. It does deal with some theories, but only the practical application of them, that would not be found in text books or come to the notice of Radio Amateurs under normal circumstances. I am not an expert on any subject because I write about them, or because I can make such a row in the Southern States on 7 MHz. at night time. All these things came about because my QTH is in a very short valley completely surrounded by hills. 120 foot towers fail to bring in the t.v. channels from Brisbane, 100 miles distant. 7 MHz. is equally unco-operative, but 3.5 and 14 MHz. (also some other bands) appear to be much better.

It is evident then that sheer necessity is the driving force behind the construction of this antenna farm. Being an antenna farm, ease of construction is a must. Such construction means light-weight gear just as it does in industry. It also means low costs. Probable gain must be in proportion to both the work involved and the costs. This is a ratio—work and costs against gain. It sets the pattern at all times. An application of this ratio to the long type of Yagi will dampen a lot of enthusiasm. It means much work—low costs—much gain and in addition an area or boom length in proportion (half an acre for 7 MHz. [0.9 acre for 13 elements], quarter of that for 14, etc.). Interested persons will now only be:

- (1) Those with adequate areas,
- (2) Scouts Clubs, etc., with more enthusiasm than cash,
- (3) V.h.f. where boom lengths cause no dismay.

Such a beam was constructed on Channel 4, necessity being the driving force for that occasion also. For the

benefit of those with little interest in Yagis, a little explanation is necessary. Maximum gain necessitates very critical tuning of the beam. This in turn means the use of gear beyond our reach. The same results can be obtained from book-values (with much less critical dimensions) by the use of more elements. For example, I spent months tuning up a 5 element Yagi and then found that I had the same spacing as those given in a text book.

For a practical explanation on the use of Yagis, I will take the position right here. Such a beam with 5 elements was already working quite well on 7 MHz. and I desired more gain. More elements meant two posts and two poles for each additional element. If I added an element at 0.1 wavelength spacing, the gain was small and in addition it could easily upset the impedance, and so be less. In the alternative method, that of re-constructing the whole antenna at 0.35 wavelength spacing, the work-cost-gain ratio was also unfavourable. Either the gain had to increase or the work decrease. Such an unlikely event actually did occur with the published reports of this combined type of Yagi. In it (now called the Long Type Yagi) the high gain of the original Yagi was retained in the front end of five elements and, without upsetting the impedance values, the additional elements at 0.4 wavelength spacing were added. Two things made this possible:

- (1) It was ascertained that it was not the number of directors used that gave the gain, but the boom length that they occupied, provided that the ratio space-length-diameter of el. was adhered to.
- (2) At that distance and spacing, the additional elements did not upset the impedance of the driven element.

These circumstances made the ratio work-cost-gain very attractive. Construction on both 7 MHz. and Channel 4 were commenced. An additional characteristic was the fact that the back-to-front ratio increased with closer spaced elements, but wider spaced elements of this magnitude gave good signal side rejection. This latter characteristic looked good as an image rejector on Channel 4. Our very local t.v. translator put beautiful images on our sets corresponding to a mountain rock face plus five timbered high spots on the ridge opposite. With the aid of an iron roof, suitably positioned, and this type of Yagi very good pictures resulted.

The antenna took only a couple of hours to construct. It was made from the plastic covered type of conduit (10 cents a foot) with No. 10 fencing wire inserted and soldered. This gave a very firm connection, and the elements could be bent at any angle. Joins of the conduit are easy with a 6 in. saw cut and a starter of another inch. This shows that quick, easily constructed beams for v.h.f. are possible for casual experi-

ments. Conduit is available in various lengths and diameters. The sag involved on the longer lengths are easily braced.

Now to return to the set-up here on 7 MHz. Steel wire of 14 or 16 gauge was used of the type used on fruit cases. The weight and strength was far beyond what was necessary, but it was available on this farm. Fence posts and poles were also available, but were also much heavier than was necessary. The insulators used were very light and efficient, being $\frac{1}{4}$ to 1 inch cut off 1 inch diameter water pipe of the polystyrene type. Higher grades may be better, but some are weather affected. Much relevant material will be found in a previous article ("A.R." March 1970). Because of the scaling factor, experiments can be changed from one band to another, although "doubling up" too much runs foul of the fact that you are not scaling up the surroundings too.

In the previous article it was shown that on 14 MHz. the forward gain dropped sharply when the antenna was lowered from quarter to eighth wavelength height. This deduction was based on the fact that W land, on which it was aimed, decreased in strength, while the JAs came up. A perusal of many text books gave little information on this problem. Most of them stop at half, but a few go to quarter wavelength height. By continuing a graph, it was assumed that the difference in the angle of radiation would be in the vicinity of 8-10° for one-eighth and one-quarter wavelength heights. Against this assumption was the extraordinary behaviour of antennas at:

- (1) Ground level,
- (2) A few inches underground,
- (3) Inside metal pipes, both open and closed,
- (4) Wire in water.

If you want a headache just read about those things. One significant fact emerged. At zero height, much gain was lost, but the signal-to-noise ratio was more favourable. If then, the gain lost by reducing the wavelength height down to one-eighth could be recovered by adding more elements, then the signal would come up more than the QRM. On such a band as 7 MHz., this matter is of major importance.

From my own experience, further experiments seemed to be futile, but a 5 element Yagi at one-eighth wavelength height on 7 MHz. had actually shown some gain. It was decided to change the experiments from 14 to 7 MHz. and accept the loss due to the lower height, because the use of 20 ft. poles made the scheme a practical proposition. As previously mentioned, the adverse ratio work-cost-gain at one-eighth wavelength height prevented further advance. When the new type Yagi was investigated it was decided to put the extra five elements on in one big heap.

A glance at the sketches show that Fig. 1 Section A is just a typical type of 5 el. Yagi except that the reflector

* Skyrings Creek, Pomona, Qld., 4568.

spacing is 0.24 instead of 0.25. That spacing was evolved using a double wire, spaced 6 inches, for the reflector. (Changing it to a single wire landed me in strife.) Section B of Fig. 1 represents the changed Yagi via the new type spacing of 0.4 wavelength, the joining director being at spacing 0.2 wavelength, but 0.4 for this also is in order.

Fig. 2 shows how the nearest two directors and the reflector were changed over to give a 4 element beam of enough gain for skeds in VK9 land (north). This 7 MHz. beam is on a compass bearing of S from a position approx. 70 nautical miles NW from Brisbane.

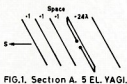


FIG. 1. Section A. 5 EL. YAGI.

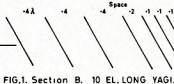


FIG. 1. Section B. 10 EL. LONG YAGI.



FIG. 2. 4 EL. YAGI IN REVERSE.

Of interest at this point is that the two-wire reflector represented quite a different effect on the impedance of the driven element than a single wire, or of that wire plus 12 inches. The factors concerned are that a folded dipole, if altered to the shape of a quad, could not have a director or reflector of a single wire. In this case, I had added three more elements to the 10 mentioned, but the gain was well down until I reverted to the original double wire reflector of 5% longer than the three-wire dipole.

From the above it is clear that the first five elements of the Yagi must be in order before the other elements are added. At this QTH the gain of the second group was far beyond that of the first group, but as explained previously, the QTH position absorbed the initial gain. The results were astonishing, especially at the other end where friends had spent years straining their ears in my direction. If I had any sense at all I would be sitting back enjoying the performance of this big beam. Instead of that, I exhibit my ignorance and show others how to equal in four days the results that took me four years to obtain.

As this article is aimed at helping (1) the bottom half, (2) the young, and (3) the inexperienced groups, much detail in construction work is necessary. It is hoped that the many problems mentioned will create a desire to solve them. It is quite clear that initially neither much money or knowledge is necessary for experimental work. For a genuine experimenter, assistance and sound technical advice is available at all times just by crying into the mike. Antenna design, progressing mathematically,

leaves many gaps that can be better probed by a practical organisation such as ours, but there is little encouragement for our new members when all awards go for DX, and quality is down in the doldrums. If we lift the quality of our transmission, then Amateur Radio will get a push-up instead of its customary push-down.

On 7 MHz. quality is useless unless it rides free of the QRM. It is here that beams become important because (1) of their effect on the signal-to-noise ratio, (2) their ability to restore the strength after other methods that were used to improve that ratio had reduced

the signal strength, and (3) the beam effect being added to the receiving improvement. If we get right down to basic requirements then we must realise that the fellow at the other end is the judge, hence we should:

- (1) Put out a good quality signal,
- (2) Put that signal well above the QRM,
- (3) Use a beam on our receiver to lift his signals up.

Although 10 elements are the basis for this article, another three were added later and an AX0 was worked on phone at R5 S6 almost immediately. At this stage, it is again emphasised that only ease of construction will make this antenna popular on 7 and 14 MHz. It is necessary to fully understand where the strain on the gear will be felt. Take a look at Fig. 3. A pole fastened to a post is similar to a long lever at B with the fulcrum at ground level, A, and moving the bottom of the post at C. Therefore ram the bottom well, also the top. Stones are useful. If using steel posts for a more permanent fixture, a wider board driven in on the inside gives a better support, but cement on the top of the ground is the best. Steel posts cost about 90 cents, 3 x 2 inch hardwood from demolished jobs is cheap and sound. These can be driven in with an axe, but in hard ground drive a crow-bar in first.

For experimental purposes, queer things have been tried. T. & G. 4-inch floor boards bolted together for the 20 ft. required have been in use for six months. Steel posts have given satisfactory service. The old type conduit is good and light. For the fixed portable — sections similar to tent poles can be joined, using either conduit or poly-

styrene piping for the joins and bamboo for the top section. If home-brew type is desired, suitable boards can be sawed by nailing to an upright 3 x 2 with the required edge protruding and the saw guided by the upright. Thin poles will have to have support from nylon string. Bricklayers' twisted nylon string has been used here for use on the elements. Small metal rings can act as pulleys for erecting the element wires and also for bracing the light poles.

With the pulley at its correct height, the minimum length of nylon string for raising the elements is such that you can reach both ends. Aligning the elements is tricky but it is quite easy if you use a plumb-bob (a big nut on some cotton). With the posts in position, work from the centres. Mark the centres of the elements with dark tape. Fasten to the centre peg and complete the element wiring for that approx. length to the end poles. With the centre pegs all in line raise the elements themselves. (It is advisable to join the centres of the dipole and three directors together at the right distance with nylon string.) By holding the plumb-bob up at arms length all elements can be aligned with respect to their pegs. Another method that I use is to hang a white cord from the reflector centre then from the centre peg of the furthest element align that reflector cord with a mark on the opposite hill, then advance toward it, aligning each element. Small changes are easily made on fixed elements by ramming the posts on one side.

For the "portables" some experimenting has been done. These particular measurements are only approximate. They were taken without a tape by lowering the end. The dowl used was holding up the tenth element of a Yagi beam on 7 MHz. The wire in use was 16 gauge steel, the length being 70 ft. plus about 5 ft. folded back and with two light insulators. Only the slightest of bends was observed in the 13 ft. of 5/8 inch dowl (two sections of 9 ft.). The type used was the kind popular for window curtains. 50 ft. of nylon string was also required. If you look at Fig. 4, it will show you how to get that dowl

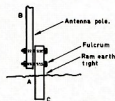


FIG. 3. POLE BASE.

up without it making figure eights. Fasten the nylon string to the top of the dowl and the wire of the element. It needs 24 ft. on each side to go to the pegs. With the dowl lying along the dotted line, follow it until the string to peg B and the element come tight. At this stage the top of the dowl will rise until the pull from the other peg (A) halts the rise. Now align the bottom for least bend in the dowl, which in this case came about 3 ft. towards the other end of the element, from the vertical position.

To join the two sections of dowel, look at Fig. 5. Again using polystyrene water pipe of 1 inch diam, cut off two sections 5 inches long. Leave A intact, cut down B for the full length and then fold it until it will slip inside A. Now take a 6 inch length this time and cut out a section 1 inch wide down the whole length (or such a width as will enable it to fit inside the second tube). The protruding $\frac{1}{2}$ inch at each end should have about five cuts $\frac{1}{8}$ inch deep to let it expand for easier entry of the 5/8 inch dowels.

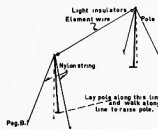


FIG. 4. ELEMENT SUPPORTS.

We come now to "spacers". Polystyrene and its class have good qualities. They are light and being 1 inch in diam. (in this case) they get over the "twisting" habit of home-brew lines. If you look at Fig. 6 it will show how to hold these slipper things while you operate on them. Fig. 7 has the holes spaced at six times the diameter of the wire for 300 ohm use—note the exact way the cut enters the hole and the side on which the nick is made. This gives a flap that can be twisted sideways to let the wires be "clipped" on.



FIG. 5. DOWEL JOINERS.

If you were to extend this drawing to accommodate one more hole in the centre between the two that are already there, you would have the 3 element folded dipole that is used in this and the former beams. These spacers were strung through the centre holes for the centre wire, then spaced in a distance of a couple of feet, then the top and bottom wires were "clipped" on. Lack of space prevents me from explaining why they don't twist even after a couple of years and probably a hundred up and down trips. For your information, warm these things in the sun. They can then be cut quite easily.

Another problem is wire. Hold the coil in the left hand and after fastening one end, walk backwards peeling the coils off to the right, say five turns, then hold it in the right hand and peel off five turns on the other side. This cancels the twist.

Now to conclude. This work is not a one-man effort. Assistance has been given freely by all Amateurs called on. The main ones concerned have been

VK2BAI, of Sydney, the "Man Friday" who has spent four years (with only one break of a few months) giving band conditions, reports, etc. at 2100 hours or 2000 E.A.S.T. Also VK4LN, of Gympie, 20 miles distant, who shouldered the responsibility of keeping everything in order and also supervised the quality of the transmissions at all times. Theory and technical advice came also from VK4XR, of Gympie. The transmitter in use was a.m. with 120 watts.

Before closing I will draw your attention to a few points:

- (1) The effect of wavelength height.
- (2) The importance of the signal-to-noise ratio.
- (3) The effect of this type of Yagi on that factor if extended to a useful limit of six wavelengths of boom length (two wavelengths used here).
- (4) The signal side-rejection characteristic.
- (5) The comparison of gain in the two sections of the 10 el. Yagi, which in my case was influenced by the valley QTH position.
- (6) The fact that the same receiving station could issue one report using a receiver for a.m., another while using an s.s.b. transceiver, and a third using his guess meter. Poor old Prof. Einstein would have thought that all his efforts in writing of the need of a common "measuring stick" had been in vain.

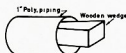


FIG. 6. PIPE HOLDER.

A little comment is necessary on the signal-to-noise ratio as it applies to both transmit and receive. I have assumed that an antenna with a good S to N ratio will act similarly on both transmit and receive. This is based on two factors, (1) the law of reciprocity (its application to beams was quoted in a previous article I think on Rhombics), (2) on a curious report received from VK2BAI where the QRM was bashed down generally, but one distant signal was still there and came up riding in on the beam. This does not necessarily mean that we broadcast our own QRM, that question should be split up into many components.

This completes this article, but in the construction field the principles of a few items should be fully understood. For home-brew lines, for example, take three pieces of the steel wire quoted and insert them in the water pipe as described and see how the cylinder construction effects both the twist factor:



FIG. 7. LINE SPACER.

and the distance apart required. For the 18 ft. dowel of 5/8 inch diam. construction, use two pins and cotton plus a straw out of the millet broom to represent the antenna problem, and how to fix it so that the strain comes on the upright in the position where it stands it best. For the join of the two sections of dowel, 1 inch piping was used because it was available, but $\frac{3}{4}$ inch can be purchased, also suitable conduit.

No work has been done on wave-length heights below one-eighth. I trust that others will see the possibilities in this changed type of Yagi. If it does not suit our methods, then we might alter our methods to suit it. If we look at our award system then we can come to no other conclusion than to regard Amateur Radio as a play-toy, not an experimental group.

★

THE REPAIR BENCH

(continued from page 11)

either go lower or return to the infinity end of the scale.

Connect the leads for the lower reading. Of course they are between emitter and collector. The negative ohmmeter lead is at the collector. This works for NPN or PNP. Put a spot of paint or fingernail polish by the collector wire so you can identify it thereafter.

LEAKAGE BY OHMMETER

The tests you've already made tell you if a transistor is leaky or shorted. It's just a matter of interpreting.

When you've established the two low-resistance readings from the base, notice the readings in the reverse directions. If they're under 10K for either junction, there is too much leakage.

If you find low readings in both directions between any two leads, that junction is shorted. If a reading between two leads shows open both ways, even on the Rx100K scale, that junction is open.

A reading less than 10K from collector to emitter, in either direction, indicates too much leakage.

Two-step method for identifying a transistor type, and base, collector and emitter connections. You need only your ohmmeter, but the transistor should be out of the circuit.

OHMMETER TESTS

Step 1.—Find transistor lead that measures low R (150 ohms or less) to both other leads; that is the base lead.

If the ohmmeter lead on the base goes to the . . . negative positive end of your ohmmeter battery, the transistor is . . . PNP NPN

Step 2.—Connect the ohmmeter for lowest R (above 10K) between the remaining transistor leads.

The negative ohmmeter lead identifies the collector.

ROSS HULL MEMORIAL VHF/UHF CONTEST, 1970-71

The Federal Contest Committee of the Wireless Institute of Australia invites all Australian and Overseas Amateurs and Short Wave Listeners to participate in this annual Contest which is held to perpetuate the memory of Ross Hull whose interest in v.h.f./u.h.f. did much to advance the art.

A Perpetual Trophy is awarded annually for competition between members of the W.I.A. in Australia and its Territories, inscribed with the name and life work of the man whom it honours. The name of the winning member of the W.I.A. each year is also inscribed on the Trophy. In addition, this member will receive a suitably inscribed certificate.

OBJECTS

Australian Amateurs will endeavour to contact as many other Amateurs in VK Call Areas and Foreign Call Areas under the following conditions.

DATE OF CONTEST

From 0001 hours E.A.S.T., 12th December, 1970, to 2359 hours E.A.S.T., 24th January, 1971.

DURATION

Any seven calendar days within the dates mentioned above, not necessarily consecutive. These periods are to be at the operator's convenience. A calendar day is from 0001 hours E.A.S.T. to 2359 hours E.A.S.T.

RULES

1. There are two divisions, one of 48 hours duration, and one for seven days. In the seven-day division, there are three sections:—

- (a) Transmitting, Open.
- (b) Transmitting, Phone.
- (c) Receiving, Open.

2. All Australian and Overseas Amateurs may enter for the Contest whether their stations are fixed, portable or mobile.

3. All Amateur v.h.f./u.h.f. bands may be used, but no cross-band operation is permitted. Operators are cautioned against operating transmitting equipment on more than one frequency at a time, particularly when passing cyphers. Cross-band operation to assist contest working is prohibited.

Such operation will be grounds for disqualification. Cross mode contacts will be permitted.

4. Amateurs may enter for any of the transmitting sections. The seven-day winner is not eligible for the 48-hour award.

5. Only one contact per band per station is allowed each calendar day.

6. Only one licensed Amateur is permitted to operate any one station under the owner's call sign. Should two or more operate any particular station, each will be considered a contestant and must submit a separate log under his own call sign.

7. Entrants must operate within the terms of their licences.

8. **Cyphers:** Before points may be claimed for a contact, serial numbers must be exchanged. The serial numbers of five or six figures will be made up of the RS (telemetry) or RST (c.w.) report plus three figures, commencing in the range 001 to 999, for the first contact, and will then increase in value by one for each successive contact. When a contestant reaches 999 he will then commence again with 001.

9. **Entries** must be set out as shown in the example, using only one side of the paper. Entries must be post-marked not later than 8th February, 1971, and clearly marked "Ross Hull Contest" and addressed to Federal Contest Manager, Box N1002, G.P.O., Perth, W.A., 6001.

10. **Scoring** for all sections will be based on the attached table. Approx. distances to be shown in the log entry as shown in the example. Failure to make this entry will invalidate the particular claim. **Operation via active repeaters or translators is not allowed for scoring purposes.**

11. **Logs:** All logs shall be set out as in the example and in addition will carry a summary sheet showing the following information:

Name.....Call Sign.....
Address.....Division.....
.....Claimed Score.....

SCORING TABLE

Distance in Miles	52 Mc.	144 Mc.	420 Mc.	576 Mc.	Higher
Up to 25 Miles	1	1	2	5	10
26 to 50 "	1	1	5	10	25
51 to 100 "	5	5	15	30	50
101 to 200 "	10	10	25	50	100
201 to 300 "	25	15	50	150	250
301 to 500 "	20	25	100	250	300
501 to 1000 "	10	35	200	300	350
1001 to 1500 "	15	100	250	350	400
1501 to 2500 "	25	125	300	450	500
2501 to 3500 "	35	200	400	500	600
3501 to 5000 "	50	300	450	550	650
5001 and over	100	400	500	600	700

Operating Dates.....(7 cal. days)
Highest Score over a 48-hour period was.....points.

Operating period:
from.....hrs. E.A.S.T. /..... /.....
to.....hrs. E.A.S.T. /..... /.....

Declaration: I hereby certify that I have operated in accordance with the conditions of my licence and abided by the Rules of the Contest.

Signed.....
Date.....

12. Entrants not abiding by the Rules of this Contest will be disqualified.

13. The ruling of the Federal Contest Committee of the W.I.A. will be final. No dispute will be entered into.

14. **Awards:** Certificates will be awarded to the winners of each section in each VK and Overseas Call Area. The VK contestant who returns the highest score in the transmitting section and who is a financial member of the W.I.A., will have his name inscribed on the Trophy which will be held by his Division for the prescribed period. A Certificate will be awarded to the contestant who shall not be the Trophy winner, and who returns the highest scoring log covering a period of any 48 consecutive hours.

Also, Certificates will be awarded for operating in the Ross Hull Contest and breaking any Australian v.h.f./u.h.f. distance record.

RECEIVING SECTION

1. Short Wave Listeners in Australia and Overseas may enter for the Contest, but no transmitting station may enter.

2. Contest times and logging of stations on each band are as for the transmitting sections, however there is no 48 hour sub-section.

3. To count for points, logs will take the same form as for transmitting sections, but will omit the serial number received. Logs must show the call sign of the station heard (not the station worked), the serial number sent by it, and the call sign of the station being worked.

Scoring will be on the same basis as for transmitting stations, i.e. on the distance between the Listener's station and the station heard. See the examples given. It is not sufficient to log a station calling CQ.

4. A station heard may be logged only once per calendar day on each band for scoring purposes.

5. **Awards:** Certificates will be awarded to the highest scorer in VK and Overseas countries.

EXAMPLE OF TRANSMITTING LOG (Brisbane Station)

Date/Time E.A.S.T.	Band Mc.	Emission Power	Call Sign	RST/No. Sent	RST/No. Rcvd.	Dist. Miles	Points Claimed
24th Dec. 0100 E.A.S.T.	52	A3(a)	VK7ZAI	59001	59004	1110	15
0105 E.A.S.T.	52	A3(a)	VK4NG	58002	57051	330	20
0230 E.A.S.T.	144	A3	VK5ZK	56003	55043	990	35
0235 E.A.S.T.	144	A3	VK3ZJO	45004	46021	850	35

EXAMPLE OF RECEIVING LOG (Perth S.w.I.)

Date/Time E.A.S.T.	Band Mc.	Call Heard	RST/No. Sent	Station Called	Dist. Miles	Points Claimed
2nd Jan. 1000 E.A.S.T.	52	VK5ZDX	58221	VK8KK	1330	15
1025 E.A.S.T.	52	VK2ZCF	58185	VK6ZAA	2040	25
1110 E.A.S.T.	432	VK6ZDS/6	57061	VK6LK/6	60	15
3rd Jan. 0500 E.A.S.T.	144	VK5ZHU	44102	VK6ZCN	1330	100

QUEENSLAND WINS R.D.

From a previous three years of low percentage participation, VK4 jumped to 17%, to win this year's contest. While generally there was increase in State scores, only an increase of 2.3% participation was registered. Assisting VK7 this year was VKOLD's entry of 3,864 points, a magnificent effort of 644 contacts.

To Queensland go our congratulations and an invitation to all Divisions to increase their entries next R.D.

—Neil Penfold, F.C.M., for F.C.C.

DIVISIONAL TROPHY WINNER

QUEENSLAND

NEW SOUTH WALES

Phone		Phone	
VK300	1102 Pts.	VK3AXJ	159 Pts.
2ATM	1089	2ACT	157
2BEC/T	876	2BBI	153
2RX	869	2AGW	151
2XT	810	2ABC	150
2ADA	742	2AMU	146
2AJY	710	2AEC	145
2RS	681	2AWW	144
2AXJ	672	2AYE	137
2AHV	623	2MW	136
2ATT	618	2BMM	136
2AZY	594	2EW	114
2APP	585	2FM	110
2BDB	558	2UJ	108
2EU	528	2JP	108
2ADJ	520	2VA	95
2BDN	508	2AW	89
2APQ	481	2ALL	87
2AIA	480	2ASV	86
2AGP	484	2AVT	83
2KM	376	2PF	81
2BIN	376	2AHE	81
2BFA	374	2ASJ	79
2AWN	365	2XD	78
2BNK	362	2BGG	78
2KR	348	2KX	75
2TS	346	2BAS	74
2AUL	335	2BJF	74
3VG	310	2EK	70
2ACZ	308	2GV	73
2BAZ	300	2ZQ	73
2BKM	297	2IJ	71
2BDC	275	2BKH	70
2WT	271	2AKV	67
2PN	269	2SG	61
2ZF	267	2BMV	54
2BMB	265	2CD	54
2BDH	258	2ATS	52
2AZE	253	2CK	51
2PC	238	2GS	48
2RU	232	2AKL	47
2AFA	230	2BNL	46
2ZB	214	2AHM	45
2RSH	205	2ANL	45
2AYF	203	2EY	41
2BEG	202	2AAW	36
2SJ	194	2P	34
2ATA	188	2AC	31
2BD	182	2HQ/P	31
2TR	179	2AAH	27
2AB	176	2ADM	27
2KA	161	2HM	25
2ADY	159	2ST	25

DETAILS OF DIVISIONAL SCORES

Division	Log Entry	Licenses	% Participation	Average Top Six Logs	Total State Points	State Score
VK2+1+9	170	2,037	8.3	1,192	41,214	4,613
VK3	82	1,838	4.7	766	23,269	1,607
VK4+9	119	694	17	1,126	33,267	6,781
VK5+8	96	746	13	1,266	30,537	5,236
VK6+9	65	468	14	1,099	17,151	3,500
VK7+0	54	232	23.3	1,672	20,243	5,328

Phone (continued)

VK2BBO/P	25 Pts.	VK2BFD	12 Pts.
2EZ	22	2OM	9
2LA	20	2ZTD	8
2AUC	19	2VH	5
2EG	18	2AGV	5
2AH	15	2ZPC	5

C.w.

VK2QL	473 Pts.	VK2RA	132 Pts.
2VH	400	2Q	77
2ANZ	364	2ZC	72
2BP	359	2IC	66
2GR	347	2BJ	63
2BCC	345	2AKK	60
2EO	227	2JY	35
2GT	185	2GW	13
2NF	175	2AND	5
2YB	166		
2ZO	149		

Open

VK2DO	1309 Pts.	VK2AGI	100 Pts.
2BO	1208	2AJQ	82
2DI	512	2OY	65
2BD	388	2AUD	39
2BBA	352	2CU	39
2AGH	294	2AL	29
2BMP	245	2BHO	28
2PU	221	2BMS	8
2PA	174		

VICTORIA

Phone

VK3VJ	976 Pts.	VK3HZ	147 Pts.
3ADVO	812	3AFI	144
3WV	808	3ACD	143
3AXV	699	3BCH	143
3ADW	653	3AER	142
3ABT	608	3ASI	138
3ASV	608	3APT	138
3SM	577	3AYF	135
3AOW	575	3EG	131
3BA	559	3AR	119
3EE	516	3BAX	113
3AHH	482	3BBB	108
3ATN	473	3AAM	106
3AZQ	466	3AHG	102
3EP	461	3PY	101
3AMK	460	3KR	100
3EDQ	459	3AV	60
3AMO	450	3PJ	73
3AKC	444	3TY	70
3YQ	385	3ARO	60
3AUN	335	3YO	57
3AQQ	321	3ZNI	56
3ZJ	319	3AJP	54
3TG	279	3V	45
3BDU	257	3AGH	44
3ACR	248	3ZQN	39
3KM	247	3ATS	34
3LV	243	3YDK	34
3BRAZ	232	3ZRL	34
3KR	196	3ABP	15
3YC	172	3TQ	14
3AUC	160	3ARA	13

C.w.

VK3AUH	302 Pts.	VK3AKT	38 Pts.
3AFN	249	3OF	31
3FC	195	3BCI	22
3AMA	162		

Open

VK3QV	688 Pts.	VK3QK	257 Pts.
3AKS	639	3AKK	235
3JI	561	3ABA	171
3DG	558	3KC	143
3APW	451	3ADP	96
3ZVU	352	3ZV	37
3SL	352	3EZ	31
3AUJ	305		

QUEENSLAND

Phone

VK4ZQ	1229 Pts.	VK4QW	126 Pts.
4EQ	1141	4EV	121
4XY	1092	4QT	120
4DZ	1018	4EZ/P4	120
4PV	986	4FK	110
4FA/P	847	4JI	80
4KH	824	4CW	81
4LZ	814	4XZ	81
4R	801	4SR	79
4IE	781	4RL	73
4LE	760	4TL	68
4VC	742	4RG	65
4UF	686	4GT	63
4AL	626	4NS	56
4BI	593	4WY	54
4BL	550	40	50
4PX	549	4JM/P4	47
4QA	566	4XO	38
4PD	550	4FP	37
4NW	528	4ZVB	35
4NY	522	4JW	29
4NQ	494	4ZKP	27
4LB	453	4VS	27
4HP	448	4YB	27
4GW	420	4GS	26
4ZC	388	4ZOC	25
4UC	322	4IO	25
4FX	302	4ZAL	21
4AR	270	4QF	20
4EB	265	4K	19
4EB	258	4KS	17
4CX	221	4ZRG	16
4CG	210	4Z	13
4GT	203	4J/P4	13
4CZ	200	4ZRT	9
4R	196	4CR	7
4RO	184	4ZBG	7
4PJ	183	4ZEA	7
4K	177	4TL	6
4WT	171	4FT	6
4FF	166	4ZFA	6
4AD	154	4ZV	5
4NO	151	4PFF	5
4UG	147	4ZFS	5
4LX/P	144	4ZRS	5

C.w.

VK4KX	454 Pts.	VK4ON	56 Pts.
4XW	380	4ZB	31
4LV	334	4FS	16
4KI	58	4RZ	15

Open

VK4LT	1145 Pts.	VK5CV/4	264 Pts.
4TL	815	4G	163
4UA	430	4BQ	17
4MY	401	4TC	14

SOUTH AUSTRALIA

Phone

VK5ZK	1358 Pts.	VK5TJ	393 Pts.
5QX	1297	5NT	376
5PT	1159	5LP	342
5BI	1147	5HM	338
5TY	1022	5ZD	332
5NN	954	5PI	324
5GV	949	5FL	306
5WV	881	5FD	301
5ZS	869	5DJ	293
5ZZ/T	737	5EP	294
5UJ	706	5LQ	284
5BT	702	5US	179
5SU	689	5G	169
5CY	547	5ZU	184
5ST	543	5GG	163
5GM	540	5W	159
5MF	529	5ZQ	138
5RR	494	5LZ	89
5GX	480	5G	86
5UN	469	5TU	80
5UK	479	5DO	80

Phone (continued)

VKSUC	..	80	Pts.	VKSCL	..	28	Pts.
SUF	..	77	"	5MA	..	28	"
SLC	..	71	"	5ZEI	..	28	"
SBS	..	68	"	5ZDX	..	28	"
SZKK	..	65	"	5ZIS	..	28	"
SXY	..	64	"	SOT	..	24	"
SVT	..	47	"	5ZLZ	..	21	"
SZK	..	40	"	5LG	..	19	"
5TW	..	37	"	5DU	..	19	"
5GF	..	36	"	5ZWW	..	19	"
5FO	..	35	"	5DF	..	18	"
SZHN	..	35	"	5CA	..	18	"
5GZ	..	33	"	5ZIS	..	8	"
5ZJ	..	30	"				

C.w.

VKSMY	..	389	Pts.	VKSRL	..	44	Pts.
SOR	..	181	"	5HO	..	30	"
SBS	..	160	"	5AU	..	28	"
5OR	..	108	"	5TL	..	20	"
5LD	..	101	"	5KU	..	15	"

Open

VKSEJ	..	899	Pts.	VKS5DV	..	369	Pts.
5FM	..	332	"	5RG	..	224	"
SAX	..	332	"	5PL	..	180	"
5IF	..	399	"	5QH	..	49	"
5OA	..	394	"	5JC	..	44	"
5VW	..	382	"				

WESTERN AUSTRALIA

Phone

VK6ID	..	1373	Pts.	VK6AV	..	74	Pts.
6CT	..	1296	"	6ML	..	68	"
6BE	..	1058	"	6HT	..	59	"
6DR	..	901	"	6RG	..	58	"
6ZK	..	860	"	6SR	..	57	"
6WY	..	908	"	6WX	..	51	"
6DA	..	889	"	6LA	..	47	"
6AB	..	651	"	6TK	..	40	"
6KK	..	453	"	6OR	..	37	"
6AO	..	394	"	6TB	..	36	"
6JY	..	362	"	6ZDB	..	35	"
6SM	..	356	"	6NM	..	33	"
6LG	..	394	"	6CN	..	28	"
6TK	..	353	"	6RU	..	22	"
6KR	..	290	"	6XW	..	22	"
6VG	..	260	"	6PX	..	21	"
6KW	..	220	"	6ZGJ	..	18	"
6WL	..	187	"	6ZFF	..	15	"
6CP	..	182	"	6PJ	..	14	"
6MB	..	185	"	6AWI	..	14	"
6DC	..	168	"	6FN	..	14	"
6RC	..	148	"	6EX	..	13	"
6RC	..	128	"	6ZAY	..	10	"
6MO	..	122	"	6ZDK	..	10	"
6NS	..	81	"	6ZFD	..	10	"
6GS	..	78	"	6ZFL	..	8	"

C.w.

VK6AI	..	382	Pts.	VK6PL	..	259	Pts.
6WT	..	372	"	6AJ	..	127	"
6GI	..	280	"	6EZ	..	13	"

Open

VK6MA	..	888	Pts.	VK6VB	..	247	Pts.
6JK	..	443	"	6NK	..	140	"
6HD	..	410	"	6CR	..	45	"
6RS	..	285	"				

TASMANIA

Phone

VK7AZ	..	1549	Pts.	VK7TH	..	132	Pts.
7TX	..	1160	"	7KK	..	129	"
7JY	..	1012	"	7SF	..	100	"
7MD	..	942	"	7VK	..	86	"
7WF	..	794	"	7LZ	..	74	"
7FM	..	580	"	7DJ	..	64	"
7ZX	..	539	"	7AB	..	45	"
7GC	..	440	"	7JV	..	23	"
7UX	..	463	"	7KH	..	41	"
7LS	..	416	"	7KX	..	39	"
7SR	..	399	"	7PD	..	35	"
7EJ	..	312	"	7JP	..	29	"
7MX	..	310	"	7ZRO	..	28	"
7BM	..	278	"	7ZIS	..	23	"
7AC	..	264	"	7ZMK	..	27	"
7AX	..	243	"	7CT	..	27	"
7CX	..	237	"	7ZAS	..	23	"
7ED	..	237	"	7ZGJ	..	23	"
7IL	..	185	"	7MR	..	18	"
7PS	..	174	"	7BQ	..	8	"
7MC	..	169	"	7ZAK	..	7	"

C.w.

VK7CH	..	420	Pts.	VK7KB	..	135	Pts.
7LJ	..	309	"	7BJ	..	78	"
7RY	..	182	"				

Open

VK7KJ	..	1295	Pts.	VK7AL	..	316	Pts.
7SM	..	1153	"	7NC	..	147	"
7PB	..	670	"	7OM	..	85	"
7ZZ	..	428	"				

ANTARCTIC

VK0LD .. 3864 Pts.

AUST. CAPITAL TERRITORY

Phone

VK1JG	..	1333	Pts.	VK1ZMP	..	17	Pts.
1AR	..	668	"	1ZHG	..	7	"
1LP	..	472	"	1ML	..	6	"
1MF	..	71	"	1ZRH	..	6	"
1YR	..	33	"				

C.w.

VK1AG .. 5 Pts.

Open

VK1BC	..	1112	Pts.	VK1VK	..	263	Pts.
1VP	..	942	"	1DA	..	153	"
1AOP	..	627	"				

NORTHERN TERRITORY

Phone

VK8DI	..	564	Pts.	VK8AZ	..	189	Pts.
8ZQ	..	293	"				

C.w.

VK8HA .. 249 Pts.

Open

VK8KK	..	1616	Pts.	VK8JS	..	369	Pts.
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PAPUA-NEW GUINEA AND TERRITORIES

Phone

VK9GA	..	1120	Pts.	VK9AG	..	215	Pts.
9RY	..	885	"	9JL	..	67	"
9BK	..	739	"	9NI	..	57	"
9XI	..	627	"	9BS	..	44	"
9AC	..	347	"	9KX	..	40	"

Open

VK9DM .. 680 Pts.

LISTENERS' SECTION

VK1	A. Blight	..	288	Pts.
VK2	S. Voran	..	1024	"
	J. Hillard, L2074	..	833	"
	P. Vernon, L2259	..	338	"
	K. Rad	..	281	"
	J. Snowdon	..	92	"
	D. Harrison	..	28	"

VK3	St. Paul's Radio Club	..	1044	"
	E. Tremayne	..	868	"
	A. Cox, L3208	..	673	"
	St. John's Radio Club	..	401	"
	D. Farquharson	..	373	"
	G. Lath	..	329	"
	W. Collier	..	303	"
	I. Delves, L3440	..	247	"
	E. Trebilcock, L3042	..	194	"
	N. Huell	..	128	"

VK4	M. Joyce, L4335	..	1110	"
	K. Cunningham, L4104	..	465	"
	R. Lonsban, L4182	..	362	"
	C. Patton, L4627	..	321	"

VK5	C. Hannaford, L5096	..	1277	"
	B. Chammen, L5118	..	773	"
	L. Earl, L5113	..	486	"
	R. Chester, L5067	..	37	"
	R. Edmeades, L5122	..	63	"

VK6	P. Drew, L6021	..	530	"
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VK7	B. Livingston, L7047	..	1026	"
	J. Everett, L7043	..	1003	"
	I. Ellings, L7038	..	318	"

CONTEST CALENDAR

7th/8th Nov.: R.S.G.B. 7 MHz. Contest (Phone).
8th Nov.: International OK DX Contest (Phone and C.w.).

14th/15th Nov.: R.S.G.B. 1.8 MHz. Contest.
20th/29th Nov.: "CQ" W.W. DX C.W. Contest.

*12th Dec. 1970, to 24th Jan., 1971: Ross A. Hull V.H.F. Memorial Contest.

13th/14th Feb.: John M. Moyle Memorial National Field Day.

*N.B.—The dates as previously published in the Contest Calendar have been altered to those shown above.

THE RADIO HAM

If you should see upon the street
A little man with dipole feet,
A train of little pipes behind,
He's a Radio Ham with a micro-mind.

His ears fan out like a radio beam,
His eyes give out with a neon gleam
And as he chews his molars oscillate
And his heart pumps blood at a video rate.

This man obtains with passing years
Infinite impedance between his ears
And finally succumbs to a heavy yolk
When he gets what he thinks is a microvolt.

The doc looks up from his microscope
And says to his nurse, behold this dope,
No trace of brain cells can I find
He's a Radio Ham with a micro-mind.



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NEW CALL SIGNS

JUNE 1970

VK1YR—Canberra Y.M.C.A. Radio Club, Station: Corroboree Park Youth Centre, Adelaide; Postal: 16 Bannister Gardens, Manuka, 2603.

VK1ZPB—P. F. Bell, 39 Larakia St., Warman, 2611.

VK1ZW—W. A. Godley, Station: 1 Gore St. Higgins; Postal: P.O. Box 15, Blamey Pl., Campbell, 2601.

VK2ADY—D. S. Hunt, 26 Mathews St., West Tamworth, 2340.

VK2ATY—L. W. A. Doolan, Station: Technical College, Newcastle; Postal: 130 Rae Cres., Kotara South, 2288.

VK2BHC—M. A. Harrison, 14 Market St., Rockdale, 2216.

VK2BRV—W. W. Allison, 98 Wardell Rd., Dulwich Hill, 2203.

VK2HR—T. F. Loider, 131 Tudor St., Hamilton, 2303.

VK2HU—G. B. Cuthbert, 2 Nioka Ave., Keirra, 2300.

VK2KI—B. R. Paterson, 30 Hyacinth St., Asquith, 2078.

VK2ZNA—M. J. Furrell, 4/183 Hopetoun Ave., Vaucluse, 2030.

VK2ZQA—R. J. Irving, 7 Lena Pl., Merrylands, 2160.

VK2ZSO—R. J. Murray, 24 Mona St., Auburn, 2144.

VK2ZVK—V. H. Kaand, 53 Edna Ave., Merrylands, 2160.

VK3AFB—D. R. Riglar, 12 Palmerston Crt., Greensborough, 3088.

VK3AZB—D. D. Harwood, 85 South Valley, Rtd. Highton, 3216.

VK3BDE—Geelong Grammar School Radio Club, Geelong Grammar School, Corio, 3215.

VK3BDE—LaTrobe University Physics Society, LaTrobe University, Bundoora, 3083.

VK3BDF—R. N. Field, 3 Mordon Crt., Nunawading, 3121.

VK3BDI—J. O. Williams, 25 Wentworth Ave., Sandringham, 3191.

VK3BDO—E. A. King-Smith, 311 Centre Rd., Bentleigh, 3204.

VK3BDP—J. E. Falkner, 17 Burgess St., Hawthorn, 3122.

VK3BDY—J. Wiseman, 20 Austral Ave., Ferntree Gully, 3156.

VK3BET—E. E. Tilley, 10 Tudor Crt., North Belconn, 3104.

VK3BFL—H. H. Chittick, 11 Lt. Myers St., Geelong, 3200.

VK3CCX—M. C. Hooper, Portable/Mobile.

VK3YCV—N. R. Laidlaw, 43 Churchill Ave., Benalla, 3590.

VK3YDG—G. J. Gill, 19 Dorset Rd., Croydon, 3136.

VK3YDR—N. Campbell, 20 Campbell St., Coburg, 3058.

VK3YDI—C. J. Jarvis, 9/105 Willemsen Rd., Oakleigh, 3166.

VK3YDP—T. J. Alder, 26 Gramatan Ave., Beaumaris, 3193.

VK3YDQ—G. R. H. Vroland, "Carlsberg", Strathgogie, 3596.

VK3YDZ—G. S. Pritchard, 32 Holland Rd., Blackburn South, 3130.

VK3YDV—K. W. Forbes, 7 Rodney St., Moorabbin, 3169.

VK3YDY—K. B. Lewis, "Kanda", Boes Rd., Hastings, 3913.

VK3YDZ—C. C. Maloney, Belgonia, Jersey St., Gladstone, 3623.

VK3ZBN—R. J. Bevers, 11th St., Mildura, 3500.

VK3ZBD—M. J. Dow, 106 Bayview St., Williamstown, 3015.

VK3ZMD—J. F. Davis, Lot 10, Cousin Dr., Bayswater, 3183.

VK4NT—N. T. Casey, 33 Herberton St., Mareeba, 4880.

VK4SZ—Sunshine Coast Amateur Radio Club, Station: 3 Bambaroo Ave., Nambour, 4560; Postal: C/o Radio Station A.C., P.O. Box 279, Nambour, 4560.

VK4ZJ—R. J. Webb, 151 Alderley St., Tooowoomba, 4350.

VK4ZJ—C/o Newmarket Gardens Caravan Park, 199 Ashgrove Rd., Ashgrove, 4060.

VK4ZBH—R. R. Hartwig, Bona Vista Ave., Biloela, 4715.

VK4ZBR—R. S. Best, 12 Ardoyne Rd., Corinda, 4075.

VK4ZGZ—T. A. W. Reynolds, 159 The Esplanade, Cairns, 4870.

VK4ZIS—I. S. Graham, Station: Dakenbar Rd., Mt. Murchison; Postal: P.O. Box 507, Biloela, 4715.

VK4ZJA—C. J. Andrews, 151 Galleys Rd., Taringa East, 4068.

VK4ZKP—K. R. Pollock, 50 Vernon St., Nunah, 4012.

VK4ZRI—A. R. Woods, 22 Stanley St., Indooroopilly, 4068.

VK4ZSD—S. D. Smith, Station: Monte Rd., Thangool, 4716; Postal: P.O. Box 16, Thangool, 4716.

VK5QE—M. M. Parks, 10 Vine St., Morphet Vale, 5182.

VK5SU—J. W. K. Adams, O.T.C. (A) Staff Quarters, Lambeth St., Ceduna, 5690.

VK5SW—R. C. Norman, 6 The Parkway, Paradise, 5075.

VK5XI—H. Hannaford, 2/10 Broughton St., Glenelde, 5065.

VK5ZFX—T. P. E. McMahon, 30 Creekview Dr., Redwood Park, 5097.

VK5ZFC—P. P. Whellum, 8 Coronation Pl., Port Lincoln, 5696.

VK5ZWB—W. B. Ricketts, Station: Section 85, Hundred of Yandarrrie; Postal: P.O. Box 70, Cleve, 5640.

VK5ZXD—J. J. Piechnick, 15 Brigalow Ave., Seacombe Gardens, 5047.

VK6AL—K. C. Ricknell, 48 Sanderson St., Lesmurdie, 6078.

VK6AZ—G. P. Clifton, 13 Morley Dr., Morley, 6062.

VK6EK—A. E. King, 4 Marloo Rd., Greenmount, 6056.

VK6ZAT—R. A. Taylor, 118 Broome St., Highgate, 6060.

VK6ZEA—K. G. Burlington, Station: Portable; Postal: C/o B.H.P. Exploration Party, P.M.B. Kalgoorlie, 6430.

VK6ZED—P. Morgan, 68 Clayton St., Bellevue, 6056.

VK7AR—H. Young, 1 Madden Pl., Devonport, 7310.

VK7IE—L. Eadie, 15A Stoke St., New Town, 7008.

VK7IH—W. I. Hooke, 302 Nelson Rd., Mt. Nelson, 7097.

VK8JS—J. P. Scougall, 13 Achilla St., Alice Springs, 5159.

VK8ZRM—R. W. Maginnis, 56 Gregory St., Parrap, 5790.

VK9AG—A. G. Mann, Station: Walungu Rd., Rabaul, N.G.; Postal: P.O. Box 110, Rabaul, N.G.

VK9AV—E. V. Avenell, St. Michael's Estate Kicta, Bougainville, N.G.

CANCELLATIONS

VK2AQF—J. H. L. Field. Transferred to Vic.

VK2AT—L. P. Crowe. Not renewed.

VK2ZHR—P. Halpin. Not renewed.

VK2ZPL—L. W. A. Doolan. Now VK2ATY.

VK2ZPB—P. F. Bell. Now VK1ZPB.

VK3DJ—J. L. Gleeson. Not renewed.

VK3EW—E. C. Wheeler. Deceased.

VK3OX—P. R. Gibson. Deceased.

VK3HV—J. W. K. Adams. Not renewed.

VK3KX—D. T. Deceased.

VK3NZ—D. E. Timms. Not renewed.

VK3AHJ—J. Vogel. Not renewed.

VK3AJK—J. Spark. Not renewed.

VK3ASY—O. W. Guy. Not renewed.

VK3AWX—S. Davies. Not renewed.

VK3AXJ—J. W. K. Adams. Now VK3KSU.

VK3ZBE—J. A. Ketchford. Not renewed.

VK3ZFO—K. M. Cocking. Not renewed.

VK3ZIR—L. A. Rourke. Not renewed.

VK3ZKR—D. R. Riglar. Now VK3AFB.

VK3ZLA—T. H. H. Chittick. Now wVK3BFL/T.

VK3ZLW—M. M. Stack. Not renewed.

VK3ZSR—K. A. Keating. Not renewed.

VK3ZTQ—C. Quin. Not renewed.

VK3ZTV—V. Avilov. Not renewed.

VK3ZYA—R. D. Young. Not renewed.

VK4VQ—E. V. Avenell. Now VK9AV.

VK4ZJ—R. J. Webb. Now VK4ZJ.

VK5WJ—C. H. Basyby. Deceased.

VK5WJ—A. B. Basyby. Not renewed.

VK5ZWS—J. B. Sparrow. Deceased.

VK6ZCB/T—K. C. Ricknell. Now VK6AB/T.

VK6ZDV—A. E. King. Now VK6EK.

VK7BHH—H. Young. Now VK7AR.

VK7ZED—L. Eadie. Now VK7IE.

VK7ZEK—W. I. Hooke. Now VK7IH.

VK8XI—B. Hannaford. Now VK5XI.

VK9DS—B. W. Smeaton. Not renewed.

VK9TB—E. W. Bastow. Not renewed.

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- ★ "CQ" Magazine, \$5.70; Three Years, \$13.50.
- ★ "73" Magazine, \$5.50; Three Years, \$11.50.
- ★ "Ham Radio" Magazine, \$5.50; Three Years, \$11.50.
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A NEW SIX METRE CONVERTER
AND A 1296 MHz. CONVERTER
For further details watch the Victorian Division Disposals Committee advertisements in "Amateur Radio"

MAILING OF QSL CARDS

Dear Sir,

Some time ago I decided to write to the P.M.G. Department on the question of postal charges and classification of QSL cards in unsealed envelopes for the purpose of direct QSL'ing.

I feel this may be of some interest to other Amateurs, who on occasions prefer to QSL direct, and who may have been in some doubt as to the relevant class and postal charges. This arose as I had received several cards in unsealed envelopes, marked "2nd class airmail" and on one occasion "printed matter only". Obviously there was a marked difference in postal charges.

Here then, is the reply from the P.M.G. Department.

—Peter P. Morrow, AX2BMP.

Postmaster-General's Dept.,
Sydney Mail Exchange,
N.S.W., 2012
3rd Sept, 1970

Dear Mr. Morrow,

First, may I apologise for the delay in replying to your letter of 12th August, 1970.

Following acceptance by the Universal Postal Union of a proposal designed to abolish commercial papers as a separate category, articles originally considered as commercial papers are now classified as letter post except the following, which may be transmitted at printed paper rates:

- (a) Letter post items exchanged between pupils of schools provided they are sent through school principals;
- (b) Pupils exercises in the original or with corrections;
- (c) Manuscripts of works or for newspapers; and
- (d) Musical scores or sheets of music in manuscript.

Consequently, there is no advantage in you sending your QSL cards in unsealed envelopes as they are not eligible for the cheaper rate of postage.

Postcards cannot be posted in an envelope or wrapper so there is no alternative here.

I cannot arbitrate, of course, upon the practices in other countries. However, Universal Postal Union ruling should impose similar treatment by all member countries.

Thank you for your interesting query and if you could arrange wider publicity for the official ruling, all to the good.

—J. Saunders, for Manager,
Sydney Mail Exchange.

TECHNICAL ARTICLES

Readers are requested to submit articles for publication in "A.R." in particular constructional articles, photographs of stations and gear, together with articles suitable for beginners, are required.

Overseas Magazine Review

Compiled by Syd Clark, VK3ASC

"HAM RADIO"

July 1970—

Inductively Tuned High Frequency Tank Circuits, W5AL. High efficiency operation of parallel 3-10002A in the 14-54 MHz. region.

A Versatile Solid State Receiver, W1FL. Tunable I.F. on 80 metres with converters for the higher frequency bands.

Low Drive Kilowatt Counter, K4EEU. IC unit to count to 16 MHz. Lengthy and detailed article. Pictures and diagrams.

Computer Processing Slow Scan Television Pictures, WAUMF.

New Look in Teleprinters, W6TJT. Seems that the old electro-mechanical machines are giving way to all electronic systems which are considerably faster.

A Solid State R.F. Signal Generator, VE5FP. Describes a unit with attenuator covering the range 0.12 to 85 MHz.

Temperature Alarms for High Power Amplifiers, W2EZY. Since overheating is one of the first indications of a malfunction, such alarms will sound off or shut equipment down before serious damage occurs.

SCR Regulated Power Supplies, W4QCC. The theory and practice.

Microwave Hybrids and Couplers for Amateur Use, W2CTK. Describes how the s.h.f. boys can roll their own instead of paying lots of money for them.

August 1970—

Interdigital Pre-amplifier and Combine Band-pass Filter, W6HTE. High performance pre-amplifier for v.h.f. receivers that features low cross modulation, low noise and excellent unwanted signal rejection.

Practical VFO, W6KBL. An interesting approach to frequency stability in oscillator circuits.

Divide by Ten Frequency Scaler, K4EEU. Describes an accessory that will increase the range of your frequency counter by a factor of ten. With this unit and the counter described in "A.R." July 1970 you can count cycles to over 100 MHz.

Computer Aided Circuit Analysis, K1ORV. A powerful tool that eliminates trial and error in circuit design.

A Tunable Audio Filter for C.W., W4JSM. Using two Raytheon RMT100 integrated circuit operational amplifiers, the 3 dB bandwidth is about 140 Hz.

A VFO for Solid State Transmitters, W3QBO. If you are tired of being rockbound, here is a neat v.f.o. featuring the Vaccor oscillator. Uses two MPF102 FETs and an HEPP5 bipolar transistor.

An Improved Six Metre Converter, K1BQT. A new approach to v.h.f. converters using FETs and a tunable local oscillator.

Improving the Interference of Communications Receivers, WA5RAQ. This author points out that sometimes the amplifier is better than the reproducer and that improvements can be made simply by improving this follow.

Quad Antenna Design Parameters, K6OPZ. The performance one obtains from any antenna is almost always determined by the final adjustments made upon the unit. This author does not agree with all that has been written. Who is right?

Modular Modules, W9SEK. Mother and daughter printed circuit boards are used to increase IC counter circuit versatility.

"RADIO COMMUNICATION"

June 1970—

This month's issue of the journal of the Radio Society of Great Britain contains a number of interesting articles.

A Keyer for G8VHF, G3MNQ. An electronic unit with only one moving part, the keying relay. Ideal for keying beacon stations. Describes down the brain, G5ON. This author points out that the keying obtained on the usual type of s.w.r. meter are often optimistic and even though you may have a low s.w.r. it is rarely 1:1:1 or less.

A Quarter Wavelength Vertical Aerial, by G3SAA. The Britisher is often said to be one who hides his light under a bushel, or to put it another way is self-effacing. This Amateur hides his vertical alongside the brickwork of his house.

Technical Topics, G3VA. Deals with "The Double Balanced Mixer," "FET Mixers," "Balanced FET converter," "All-Transistor Transmitters" including some mention of VK7RG "Amateur Radio" and "The Australian EEB," cathode modulation using transistors is also covered in some detail.

Fut a Transistor in Your Cathode (2). G3SBA continues his article on getting something for almost nothing. Of course this technique has been used before to power the low power front-end stages of a communications receiver undergoing modification to solid state on a stage by stage basis.

T.V.I. Tips, G3JGO. For those plagued by the stuff.

Using a Hopeful Future, G5UM. Sixteenth V.h.f./U.h.f. Convention report.

July 1970—

A 100 M. Linear using High Voltage Transistors, G3UFW. Describes some of the possible tricks for increasing power to transistor rigs.

A Narrow Band F.M. Exciter for the V.M.F. Bands, G3ISZ.

Fut a Transistor in Your Cathode (3). G3SBA. A hybrid driver stage for an s.b. transmitter. **Technical Topics**, G3VA. This is a monthly feature conducted by Pat Hawker which provides a prels of a number of articles which have appeared in the various journals, not necessarily Amateur, but which appears to be of interest to a goodly number of the fraternity.

Oscillator Noise and its Effect on Receiver Performance, G3JGO. With a title like that, what else can one say?

Solid State Modules, 2 M. Converter, G3GGK and G3GDD. Noise factor better than 2 dB. Gain 35 dB. D.c. supply 12-15 volts, I.F.s available: 4-6 or 28-30 MHz.

The Decibel, G3BBO. The newcomer to electronics usually has difficulty in understanding the dB. It is explained here once again for those who need it.

"RADIO ZS"

June 1970—

A Parenthetical Fairy Tale, W1JQB. **Electronic Time Meter for the Darkroom**, by ZS1CA.

About Making S.W.I. Reports, ZS1RR. **Six Metre Conversion of the B-14 Transmitter Receiver**, ZS1IM. This unit originally operated in the range 60-85 MHz. on three pre-set crystal controlled channels.

Improvements for the FL100B S.B.S. Transmitter, ZS1CK. This author states that his unit was unusable and unusable is nearly impossible to improve the in-built v.f.o. without major surgery. He therefore built an outboard v.f.o. and made certain other mods to improve the performance.

July 1970—

Some Linear Considerations, ZS5HF. A discussion of what happens if a "linear" is not and how to make it so.

Q-Code. Tells you what these three letter groups mean.

The G3NUG Triband Single Feed Quad. Dimensioned sketches only.

All Hams Are Bragariats, ZS1ACD. Perhaps we are all bragging in certain directions.

F.H.C. The Flying Ham Club.

"73"

July 1970—

An Improved Method for the Transmission of Colour Information by Slow Scan Television, W4UMF. Those who are interested in colour t.v. should follow up on this one for themselves.

World-Wide L.T.U. Prefix/Call Area List, W1SWX. What can I say?

The Super Audio Pack, K6MVH. When disaster strikes there is no substitute for rapid traffic handling. This facilitates person to person contact.

How to Build a Keyer (and retain your appliance operator status), W9KKJ. VKs would probably find that 2000 type relays provided the necessary basis.

A Two-Channel Search and Lock for F.M. Receivers, W3DTN. This simple gadget turns a two-channel rig into an automatic scanning unit and provides the added capability of locking on a channel where activity is sensed.

A Look at Allied's Portable F.M. Receivers, K6JW. The Japanese have a reputation for the mobile bands but one covers 2 metres. They are considered to be good value although not really ham rigs.

500 MHz. Mighty Mite, K6VXL. Maybe one should say the littlest transmitter.

Cheaper Six Metre Half Gallon, K1CLL runs 500 watts on 60 MHz.

High Performance Power Supply using an IC Regulator, K6ECF.7. Move over voltage regulators.

Latham Island DX-pedition, 5H3LV and 5H3KJ. Good hamming holiday.



Sub-Editor: ERIC JAMIESON, VK5LP
Forreston, South Australia, 5233.

Closing date for copy 30th of month.
All Times in E.S.T.

AMATEUR BAND BEACONS

VK4	144.390	VK4V9, 167m. W. of Brisbane.
VK5	53.000	VK5VF, Mt. Lofly.
	144.800	VK5VF, Mt. Lofly.
VK6	52.006	VK6VF, Tuart Hill.
	52.900	VK6TS, Carnarvon.
	144.300	VK6VE, Mt. Barker.
	145.000	VK6VF, Tuart Hill.
	435.000	VK6VF, on by arrangement.
VK7	144.000	VK7VF, Deception.
VK9	146.000	VK9XI, Christmas Island.
ZL3	146.000	ZL3VHF, Christchurch.
JA	51.895	JA1IGY, Japan.
W	50.091	WB6KAP, U.S.A.

An interesting letter this month from Kerry Adams, AX8SU, who is located at the O.T.C. Satellite Station, Sedona, on the Arizona-Sonora border, tells us that he has moved to a new home in Paradise, Arizona. Kerry reports that at the installation the antenna system is four Amateurs, two being Ken on v.h.f. and two on h.f. The antenna is presently set-up in an FT200 for h.f. to TH3JR at 40 feet. An EFV500 is even ordered and in readiness. The FT200 has been equipped with a 16 meter antenna for portable use. The 16 meter antenna is 4 elements at 45 feet, while 10 element 2 metre beam is mounted at 48 feet. Feed lines are all 1/2" and the antenna is mounted on a 3" x 4" base. Some problems have existed with high winds snapping the telescopic mast with all that weight hanging up top, but Kerry says the mast is now forward of the antenna and the DX contacts on the 16 meter frequency are 144,200, 144,400 and 144,800 MHz, the last being most used. (I might suggest that the antenna be set up for 144,000 MHz for the most Amateurs' converters and beams are optimum in lower portion of band—5LH). Kerry also plans using the QEQE/40, etc. transmitting

Bob VK3AOT advises the bands have been quiet for some time now, although Lou VK-3ZYD has been having successful t.v. transmissions on 432 MHz., using home-brew solid state t.v. camera, 2-1 interlaced scanning, transmitter grid modulated QQE66/40, receiver uses VK3 432 MHz. converter.

The VK3ZCJ day on 27th Sept. attracted 7 portable stations on bands between 8 and 432, but due to poor conditions no contacts were made with VK5 stations. Here in VK3 there was a lot of activity on 20m and 30m bands, but again under quite foul conditions. Heavy and widespread rain fell over most of the likely operating areas all day on the Saturday (26th) and the day after, with a few sunnier intervals and generally shocking conditions. However, there was a lot of fun and one group under the call sign of VK3ZDX/B was noted with more than 100 contacts on 20m and 30m bands under the conditions. John VK5QZ and myself did not get under way until the afternoon session, but ran up 100 contacts in 3 hours using 100w and 10m antenna. This was the type of activity under such poor conditions.

examination by Colin VK5ZKR, Garry VK5ZGR and Chris VK5ZFA. Such happenings are an acid test for the degree of indoctrination of v.h.f. interest. It would certainly be a tragedy for v.h.f. should they desert the bands; we all hope not. However, congratulations to you all.

MEET MR. MOONBOUNCE

The following is extracted from "Break-In," the official publication of N.Z.A.R.T., for which we thank them, the item being of general interest to v.h.f. operators.

"At this time of writing, John has worked Sweden, SM7BAE, no less than 21 times! (This must surely be some sort of record!) and the U.S.A. (Iowa), K0MQS. He has been heard by VK3ATN, many Ws and VETBQH, and on the local scene, ZLIMO. But the most tantalising one is that he has had partial two-way contacts with Mike Staal, K0MYC, for three years without ever making it a 'real' contact. Tenacity must pay off here.

"June 10: Sixth consecutive QSO with SM7BAE. Just missed with K6MYC. John was hearing him well, but Mike could not quite get a signal report from John. June 13: Same again with K6MYC, but this time John could not get the signal report. Heard V7BQH quite well, but it looks as if he needs 1 or 2 dB. more at his end (he is using 80 element collinear—needs a 160 element—Ed.) Quite a record, isn't it?"

Mike quickly note to advise that the first N.Z. call was received on 12/1/70, from the N.Z. callbox between 0300 and 0400 July 7, 1970, GMT, from IZ1MRY in San Jose California, and IZ1MRY made a two-way QSO on 144.504.5 via IZ1MRY. IZ1MRY was very friendly and a most generous amount of pleasure because Mike has been a great source of encouragement to me over the past few years in my MB efforts—also it was a very good first experience for me. IZ1MRY because I first heard KEMYC in 1965/66 and he has heard me since 1967. We have another sked tomorrow and VE7BQH is also taking part. IZ1MRY is a very good skater and skates well during today's sked for about 20 minutes, so with a little luck I may make the first N.Z.-Canada 2 metre QSO. Other skeds are being made with IZ1MRY and IZ1MRY is a mutual time with France is PR1LY Limited.

"As John says, it is very difficult to obtain perfect frequency stability when keying a large v.h.f. transmitter, but believe it or not, John keys the d.c. (battery) supply lead to the 14 MHz. crystal oscillator only. He found this to be the only method which gave him perfectly chirp-less keying. John mentions that a moment's thought will show that even a keying change from 10 to 20 Hz. during keying will put considerable ripple right into the basepass of the audio filter. A chirp as small as this is not even noticed in a 500 Hz. wide filter at normal b.f.n. mth.

"John adds: 'However, the same could be said of any v.f.o.! I am sure that the circuit used has little bearing on the stability obtainable unless one has the patience to persevere with the temperature characteristics of the gadget in your particular environment.'

"John adds a final comment to those contemplating EME or MS work. "I have found during recent skeds that better weak signal results have been obtained since changing the I.F. bandwidth from 500 Hz. to 2.3 KHz. When used in conjunction with a narrow band tuned circuit, the noise level is reduced to a level more even noise spectrum—apparently the narrow 500 Hz. filter maintains a slight ringing tendency on noise pulses and, of course, the following audio filter magnifies the result to the stage where the theoretical signal-to-noise ratio of reduced bandwidth is not realized in practice."

NEWS FROM THE NORTH

Doug VK8KHC in Darwin sends an interesting letter about happenings to the north of Australia. Life reports conditions have been little short hectic since the end of May; the weather has varied from 6 metres most nights. The S2 MHz backscatter net on 14130 kHz is working perfectly with stations calling at intervals of 7 minutes or so. It's regularly heard being JAILZC, JAIMRS, KA-SSWV, HJLWV, VSDDA, VSGBF, VKDCE, VKQBBB, VKWKRO, VKLASZ, VKAUA, VKDJD, VKRKC, VKYUO, etc., as well as many others who are listening to the two main interests: (1) nightly "pipe-line" between Darwin and New Guinea on 6 metres, and such-and-such other stations that allows Dave K8STH to make his ten-nan watt station hearable for hours on end, and (2) worked NGAUS on VKWKRO at Ayr on 19th Sept. at 9 pm during which Doug was able to pick up some very faint signals from VKKAU! Present procedure is to monitor 14130, stop if anyone is listening @ 6 metres, always assume it will be a reply, and away they go!

VK8KHC

Continuing with Doug's news, he reports that the HL9W1 runs his beacon on 50.100 MHz. up to about 1930 daily and all day, then changes frequency to 52.010 MHz. from then on. It is c.w. and s.s.b. and has a 15 second break-in period as announced. Doug would also like to know if there is any way of stirring DU and KKH prefixes to get on 6 metres, there are plenty of them but seemingly little interest.

And that's just where these notes finish, there is no more news! Thought for the month: "If I were a godfather wishing a gift on a child, it would be that he should always be more interested in other people than in himself. That's a real gift!" T3, Eric VK3LP, the Voice in the Hills.

MEET THE OTHER MAN



Ross VK4RO

Meet Ross VK4RO, ex-VK4ZRV, of Ayr, 50 miles south of Townsville in North Queensland. First licensed in 1960, Ross operates in the 32 and 144 MHz. bands plus 10 through to 80 metres. On 32 MHz. he runs 400 watts p.e.p. using a 3-400Z in the final to a 4 element Yagi up 10 feet. The converter and tunable i.f. together are an SB-110A Heathkit, and he has worked VK1, 2, 3, 4, 5, 6, 7, 8, 9 and ZL4. (This is a surprise, most others have worked ZL1, 2 and 3 but no 4!) In addition he has worked all JAI to JA0 inclusive and KR8.

On 144 MHz. Ross runs 10 watts to a TT15 with a 10 element Yagi up 40 feet, with an R.T.V. & H. converter to a KW77. He has not worked out of VK4 so far, and being about 900 to 1,000 miles from the main centre of 2 metre activity, makes it hard to do very much. His location is 13 feet above sea level. However, when the occasion permits or conditions demand, Ross is able to go out portable and has a site about 10 miles south of Ayr 600 feet high, but the last 50 feet needs gear to be carried! Power is from a 300 watt a.c. alternator and uses the SB-110A equipment on 6 metres and 1925 transmitter and converter on 2 metres, 5 element beam for 6, 10 element for 2 metres.

Ross is a member of the W.I.A., President of Townsville Radio Club for two years, and is an electrician by occupation. He has recently returned from a trip to Japan, Taiwan and Hong Kong with his brother Dale VK4ZDG and Peter VK4ZPL. They met about six JAI 6 metre operators and were given a "royal" welcome. Thoughts for future activity include plans for 400 watts p.e.p. a.s.b. on 2 metres, then on to 2 metres i.m. mobile, and the distant future 432 MHz.



Doug VK8KK

Now we go to a fresh State and get some news from Doug McArthur, of 9 Bulbul St. Ludmilla, Darwin, under the call sign of VK8KK, previously VK5KK. First licensed in 1958, Doug has been a very keen v.h.f. type ever since. He was a former President of the VK5 V.h.f. Group, and when his work as a shift supervising technician with the Radio Australia booster station took him to Darwin plenty of radio gear went with him or has been sent up since. He made his presence known by spending some time as President of the Darwin Radio Club. His location is 1400 feet above sea level and he holds certificates for V.H.F.C.C. and W.A.V.K. awards obtained while in VK5. Other interesting details re VK8KK were given in the V.h.f. Notes for October. Taken overall, Doug must lead a very busy life, so I am sure we all wish him well in the cause of Amateur Radio.

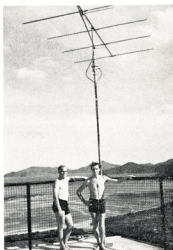


Geoff VS6DA

Geoff VS6DA photographed at his QTH in the New Territories of Hong Kong, holding a QSL from Doug VK8KK which records their 6 metre two-way—believed to be the first ever Hong Kong/Darwin—contact on 50 MHz.

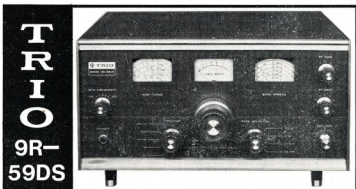
The QSO took place on 2nd June, 1970, at 1145 GMT, and was perfect 5 x 9 copy at both ends. VS6DA's 6 metre gear is on the left of the photo and is the Yaesu FTV650, in conjunction with the FLDX400. The beam is a 5 element wide spaced by Maspro, whilst Doug uses a home-brew transverter into an FTDX400 with a 9 element Yagi.

Geoff lives permanently in Hong Kong and is a pilot for an airline based there. He flies into Perth, W.A., from time to time and enjoys eyeballing with the VK6s. You will find him on 14.180 MHz. when he's not on duty, ready to try for more VK DX on 6 metres.



John VK8ZCW with Geoff VS6DA

John VK8ZCW (on the left) with Geoff VS6DA at his QTH overlooking the sea in the New Territories of Hong Kong. The 6 metre antenna shown is the one used in the recent two-way QSO between Darwin (VK8KK) and Hong Kong. John was able to call on Geoff recently whilst vacationing in the Far East and deliver personally the 6 metre QSL card from VK8KK.



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555	VWZ	623	WASZB	691	WASZB
556	WAOAH	624	KXARM	692	AXZBAZ
557	WIHOH	625	WZHF	693	ZL2LAGO
558	GWSPF	626	WYRBO	694	WYRBO
559	VEZSD	627	AXQAQ	695	G6VY
560	GZBFC	628	WOCDC	696	WASZB
561	JHIMT	629	WBZWS	697	ZM1AN
562	WOLG	630	WQPI	698	WQPI
563	VEZTL	631	AX3XD	699	AX3ACD
564	WQZJ	632	GHZ	700	WVWQ
565	WYV	633	AX3AC	701	WVWQ
566	VE3CBG	634	KYUYI	702	ZM1DS
567	AX3OW	635	W6KDK	703	WBWCE
568	ZM3GS	636	KL2DNE	704	WYRBO
569	DKZMO	637	AX2AFA	705	MP4BHL
570	AX3AAO	638	AX3ZZ	706	KI2OR
571	KSSSN	639	AX3AKC	707	AX3AUN
572	AX3AZ	640	3BRZC	708	ZM1BUO
573	WOFU	641	AX2ARQ	709	VYSAI
574	W6WUP	642	AX4EZ	710	AX3AR
575	WVWQ	643	AX3AC	711	WVWQ
576	WIRAN	644	WASJCJ	712	ZL2AMP
577	DJ3JK	645	AX3ASI	713	WASHUP
578	GXJN/M	646	AX3RJ	714	G6VY
579	WQZJ	647	WAEDEC	715	WVWQ
580	JAGLU	648	KL7GSC	716	VEZBPP
581	AX3AU	649	ZM3AH	717	WVWQ
582	WVWQ	650	ZM3ADN	718	WVWQ
583	W6GKM	651	DJ4PI	719	WRYKY
584	WIKO	652	AX3GG	720	WASAS
585	WVWQ	653	WVWQ	721	VESAZ
586	K4IEP	654	AX3RG	722	W3RZ
587	W8ETP	655	W4ACGD	723	KALAN
588	LUSAQ	656	AX3AMA	724	AX3BPG
589	GK3KA	657	AX3F	725	WADHDS
590	EL3CB	658	AX3KR	726	GXRXC
591	WAZCEP	659	G3VQT	727	3BRVC
592	WZNEP	660	DJ3EN	728	WASVSW
593	W8VHY	661	9G1GT	729	AX4TT
594	W3CJF	662	AX3AAL	730	KQ9QY
595	W6KDM	663	WVWQ	731	VEAFA
596	WBLN	664	VE3RCS	732	WBRZDF
597	VE4XQ	665	OK2SF	733	KG6E
598	W4WSF	666	AX3BDH	734	WZSWR/M
599	K0BDW	667	K0BDW	735	JL3ADN
600	K5BPT	668	WB4MEK	736	DJ2MV
601	W2CUC	669	DL8MM	737	AX4RT
602	WVWQ	670	WVWQ	738	WVWQ
603	W6VEM	671	AX3GA	739	WRRKP
604	XE1ER	672	WIIMP	740	WASHGV
605	W2PFL	673	WRAQZ	741	HS4ADH
606	3BRVC	674	AX3AUL	742	AX4EY
607	K4DXO	675	VE3BSP	743	GGLM
608	WBHXC	676	G3UGC	744	ZL2AK
609	W3ABH	677	CT1LN	745	WVWQ
610	HBBAAA	678	AX3BBC	746	AX3GR
611	AX3UG	679	AX3AO	747	WVWQ
612	DL8OX	680	WVWQ	748	HBBAAA
613	DL8QB	681	W4WVG	749	WVWQ
614	WB6DXU	682	W4ZNRD	750	WVWQ
615	W8VYU	683	WABTJ	751	VE3BSJ
616	VQ8CZ	684	AX3U	752	ZM3AC
617	ZM1BI	685	AX3BDN	753	AX3IE
618	WTEKM	686	AX3ATM	754	G3GHE
619	ZM3AC	687	AX3MW	755	AX3ACT
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TO MALTESE EMIGRANTS

3914 Casgrain Drive,
Windsor, Ontario, Canada.

Editor "A.R.," Dear Sir,

A large number of Maltese emigrants settled in Australia during the last 25 years. The Maltese Amateur Radio International Society is now being formed and looking for Maltese Amateurs in every part of the world. With a population of over 100,000 Maltese Australians, I am sure that a number of these are either Ham or will be interested in knowing that the M.A.R.I.S. is now being formed.

I am hoping that you will be able to help by giving us some space in your Federal magazine "Amateur Radio" which goes to every affiliated club in Australia and to about 4,000 Ham across the country.

We are planning to select the Directors in the early part of next year and we are hoping to have a Director from each continent. We are setting the bar by law, frequency of meetings, affiliations with various wireless institutes, etc. We also have a supply of three coloured QSL cards which will be available at a very reasonable cost to all members.

Thanking you in advance, and hoping that the response will be great, for further information, anyone can write to me at the above address.

—G. N. Muscat, Founder/Director.

[Licences are available to all naturalised migrants.—Ed.]

W.I.A. D.X.C.C.

Listed below are the highest twelve members in each section. Position in the list is determined by the first number shown. The first number represents the participant's total countries less any credits given for deleted countries. The second number shown represents the total D.X.C.C. credits given, including deleted countries. Where totals are the same, listings will be alphabetical by call sign.

Credits for new members and those whose totals have been amended are also shown.

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112	VK4HF	143/150
113	VK4ZK/0	104/104
113	VK3AMU	99/103

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112	VK3AGH	274/300
113	VK4FJ	290/315
114	VK4HR	289/311
115	VK3AGH	288/311
116	VK3AKP	288/311
117	VK4KES	300/313
118	VK4RQ	165/177
119	VK4PZ	224/235
120	VK3AMK	226/226
121	VK3AGH	226/226
122	VK3AGH	226/226
123	VK3AGH	226/226
124	VK3AGH	226/226
125	VK3AGH	226/226
126	VK3AGH	226/226
127	VK3AGH	226/226
128	VK3AGH	226/226
129	VK3AGH	226/226

AMENDMENTS:

Cert. No.	Call	Total
111	VK4RQ	137/138
112	VK4HF	143/150
113	VK4ZK/0	104/104
113	VK3AMU	99/103

OPEN

Cert. No.	Call	Total
111	VK4RQ	137/138
112	VK4HF	143/150
113	VK4ZK/0	104/104
113	VK3AMU	99/103

MORE MISSING NAMES

Editor "A.R.," Dear Sir,

The No. 4 person in the photograph is myself and I was owner and operator of station 2ED at Walton Crescent, Abbotstford Point, N.S.W., with a length of 20 metres.

I believe that No. 2 person in the front row was Mr. C. P. Bartholomew, he was President of the Wireless Institute of N.S.W., and also a Director of Amalgamated Wireless, Australasia Ltd. as well as a Director of Beard Watson & Co. Ltd.

Suggest that No. 8 person in the back row was Sid Colville, of Colville & Moore Radio Supplies, Rowe Street, Sydney.

—Harold R. Gregory

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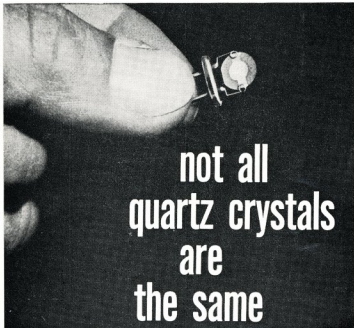
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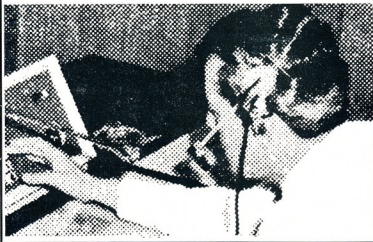
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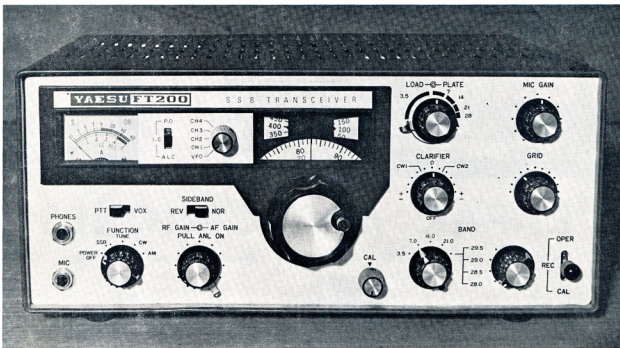
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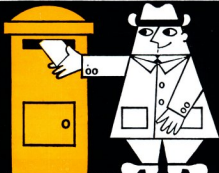
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